

# Achieving ultralow leakage current in Schottky-MIS cascode anode lateral field-effect diode based on AlGaIn/GaN HEMT

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Received 28 June 2024/Revised 26 August 2024/Accepted 17 October 2024/Published online 18 December 2024

**Abstract** In this paper, we design and fabricate a Schottky-metal-insulator-semiconductor (MIS) cascode anode GaN lateral field-effect diode (CA-LFED) to achieve ultralow reverse leakage current ( $I_{LEAK}$ ). The device based on AlGaIn/GaN high-electron-mobility-transistor (HEMT) includes a normally-off MIS-controlled channel that is cascoded with a high barrier height Schottky contact. At reverse bias, the high electric-field is effectively prevented by the normally-off MIS-controlled channel edge. Together with the high barrier height Schottky contact, this feature significantly suppresses the  $I_{LEAK}$ . Supported by the device fabrication, the CA-LFED with high breakdown voltage (BV) > 600 V shows an ultralow  $I_{LEAK}$  of  $3.6 \times 10^{-9}$  A/mm as well as a low forward voltage drop ( $V_F$ ) of 2.2 V. The performance suggests that the CA-LFED can be a promising candidate for ultralow  $I_{LEAK}$  and better  $V_F$ - $I_{LEAK}$  trade-off GaN power diode applications.

**Keywords** Schottky-MIS cascode anode, lateral field-effect diode (LFED), ultralow reverse leakage current ( $I_{LEAK}$ ), forward drop and reverse leakage trade-off, AlGaIn/GaN HEMTs

**Citation** Wang F Z, Gao C H, Ding G J, et al. Achieving ultralow leakage current in Schottky-MIS cascode anode lateral field-effect diode based on AlGaIn/GaN HEMT. *Sci China Inf Sci*, 2025, 68(1): 112403, <https://doi.org/10.1007/s11432-024-4197-y>

## 1 Introduction

Advances in power electronics technology require the development of high-efficient diode devices [1]. The GaN material has become a competitive candidate for fabricating high-power and high-frequency devices because of its wide band-gap, high electron mobility, and high critical electric-field [2–4]. The lateral diodes based on AlGaIn/GaN high-electron-mobility-transistor (HEMT) can be used in the monolithic integrated power applications [5]. Many GaN lateral diodes have been proposed to realize the low reverse leakage current ( $I_{LEAK}$ ) as well as low forward voltage drop ( $V_F$ ) [6–9]. Conventional Schottky barrier diode (SBD) inherently has a low cost fabrication process [10]. Nevertheless, the Schottky contact directly withstands the high reverse potential and then presents high  $I_{LEAK}$ . Moreover, the high resistivity AlGaIn barrier exists between the two-dimensional-electron-gas (2DEG) and Schottky contact, which seriously degrades the  $V_F$  of the device. The principle of the lateral field-effect diode (LFED) based on AlGaIn/GaN HEMT is reported to reduce the  $V_F$  [11]. In the GaN LFED, the anode consists of the electrically shorted source Ohmic contact and gate electrode of a normally-off GaN transistor, while the cathode is the Ohmic drain [12,13]. However, this low  $V_F$  architecture often results in a relatively high  $I_{LEAK}$  due to the contradictory relationship between the  $I_{LEAK}$  and  $V_F$ . The GaN lateral diodes with various technologies,

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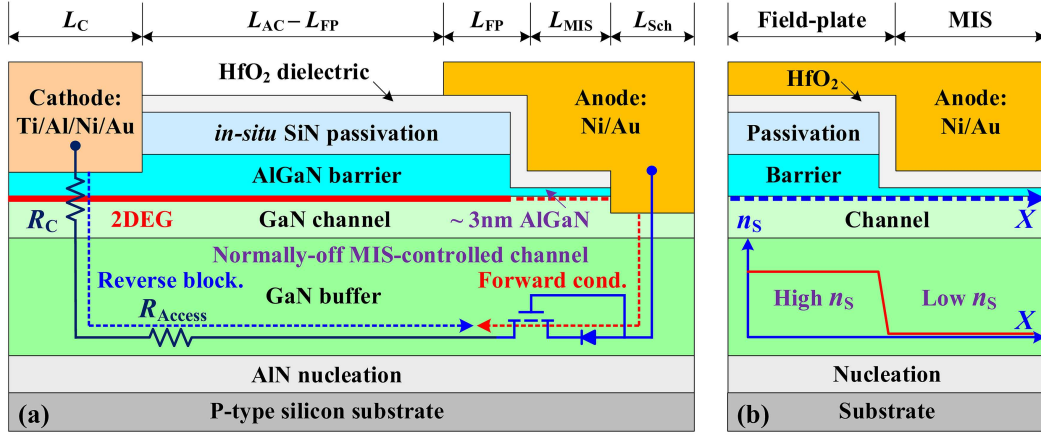


Figure 1 (Color online) Illustration of (a) device structure and (b) 2DEG density of the CA-LFED.

Table 1 Epitaxial structure and dimensional parameters.

Symbol	Quantity	Value
$L_{Sch}$	Schottky anode length	45 $\mu\text{m}$
$L_{MIS}$	MIS anode length	1.5 $\mu\text{m}$
$L_{FP}$	Field-plate (FP) length	2.0 $\mu\text{m}$
$L_{AC}$	Anode-to-cathode length	4.5/9.5/19.5 $\mu\text{m}$
$L_C$	Cathode length	45 $\mu\text{m}$
$W$	Width of the device	10 $\mu\text{m}$
$t_{HfO_2}$	HfO <sub>2</sub> dielectric thickness	16 nm
$t_{pass}$	SiN passivation thickness	54 nm
$t_{ba}$	AlGaN barrier thickness	13 nm
$t_{ch}$	GaN channel thickness	150 nm
$t_{bu}$	GaN buffer thickness	4.0 $\mu\text{m}$
$t_{nu}$	AlN nucleation thickness	200 nm
$t_{sub}$	Silicon substrate thickness	800 $\mu\text{m}$
$x_{ba}$	AlGaN barrier Al composition	0.25

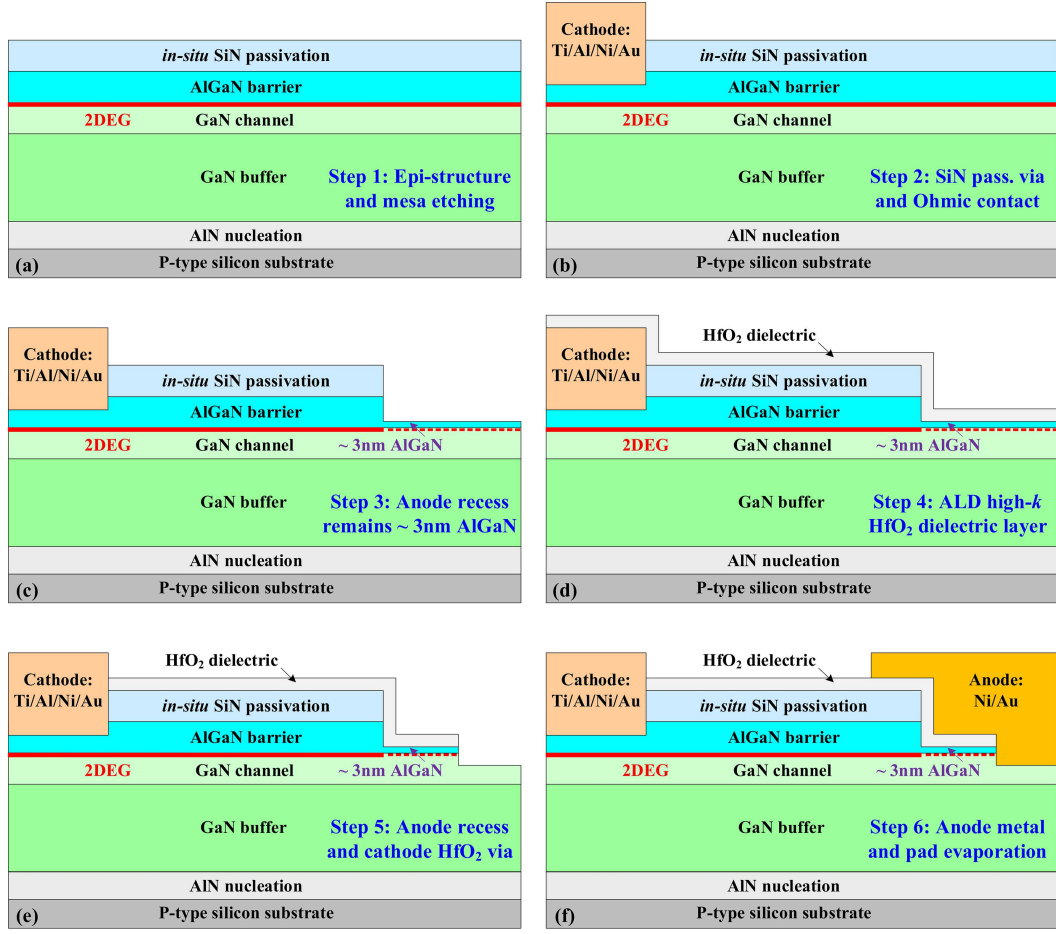
such as the recessed anode [14–16], anode field-plate (FP) [17–19], and novel epitaxial structures [20–22], are presented to suppress the  $I_{LEAK}$  and meanwhile maintain the low  $V_F$ .

In this article, we experimentally demonstrated an ultralow  $I_{LEAK}$  Schottky-MIS cascode anode LFED (CA-LFED) based on AlGaIn/GaN HEMT. Cascoded at the device anode, the normally-off MIS-controlled channel and high barrier height Schottky contact prevent the high reverse electric-field and significantly suppress the  $I_{LEAK}$ . Verified by the device fabrication, the proposed CA-LFED shows an ultralow  $I_{LEAK}$  of  $3.6 \times 10^{-9}$  A/mm and a better  $V_F$ - $I_{LEAK}$  trade-off.

## 2 Device structure and fabrication process

Figure 1 illustrates the device structure and anode 2DEG density ( $n_s$ ) of the CA-LFED. To ensure good electrical properties of the fabricated devices, the in-situ SiN passivation is utilized in this work [23]. Table 1 lists the epitaxial structure and dimensional parameters of the device. The CA-LFED features the cascaded normally-off metal-insulator-semiconductor (MIS)-controlled channel and high barrier height Schottky contact. Its equivalent circuit could be considered a normally-off HEMT and an SBD with the anode-to-gate and cathode-to-source connections. The HfO<sub>2</sub> has a high dielectric constant (high- $k$ ). At reverse bias, the normally-off MIS-controlled channel with a Ni/HfO<sub>2</sub>/AlGaIn structure can fully deplete the 2DEG underneath. With the contribution of high barrier height Ni/GaN Schottky contact, the high reverse electric-field can be prevented to achieve an ultralow  $I_{LEAK}$  in the CA-LFED. Additionally, the 2DEG density of the normally-off MIS-controlled channel can be recovered at a low forward bias because of its relatively low threshold voltage ( $V_{TH}$ ), ensuring a low  $V_F$  of the CA-LFED.

Figure 2 presents the fabrication process flow of the CA-LFED. At first, the device fabrication started



**Figure 2** (Color online) Fabrication process flow of the CA-LFED. (a) Step 1: epi-structure and mesa etching; (b) step 2: passivation via and Ohmic contact; (c) step 3: anode recess remains 3 nm AlGaN; (d) step 4: ALD high- $k$  HfO<sub>2</sub> dielectric layer; (e) step 5: anode recess and cathode HfO<sub>2</sub> via; (f) step 6: anode metal and pad evaporation.

with the epi-structure preparation and mesa etching. The SF<sub>6</sub>/CHF<sub>3</sub> and the Cl<sub>2</sub>/BCl<sub>3</sub> mixture gases were used to etch the in-situ SiN passivation and AlGaN/GaN hetero-structure, respectively (Figure 2(a)). The atomic force microscopy (AFM) indicated that the etching depth is about 500 nm. Then, to form the cathode Ohmic contact, the Ti/Al/Ni/Au (20/150/55/45 nm) metal stack was deposited after etching the in-situ SiN passivation (Figure 2(b)), followed by the 850°C annealing for 30 s in the N<sub>2</sub> ambient. The transmission-line-model (TLM) results for the sheet resistance ( $R_{SH}$ ) and Ohmic contact resistance ( $R_C$ ) are 580 Ω/sq and 1.5 Ω·mm, respectively. After that, for the anode recess structure of the normally-off MIS-controlled channel, the in-situ SiN passivation and the AlGaN barrier are etched with the remained AlGaN about 3 nm (Figure 2(c)). After etching the anode, the AFM morphology demonstrated in Figure 3 suggests that the etching depth is estimated to be about 64 nm. The 3 nm thickness AlGaN barrier beneath the MIS anode is challenging to control as it is a very small value. The variation in the etching process may cause the different etching depth, resulting in the carrier density variation under the MIS anode and impacting the  $I_{LEAK}$  and  $V_F$  performance of the CA-LFED. Here an ultralow power (5 W) BCl<sub>3</sub>-based etch technique is developed to achieve an AlGaN etching rate of about 1.2 nm/min, which is adopted to accurately control the recess depth and guarantee the performance uniformity. Next, a 16 nm high- $k$  HfO<sub>2</sub> dielectric was then deposited in the atomic layer deposition (ALD) system (Figure 2(d)). Subsequently, the remaining 3 nm AlGaN barrier, GaN channel, and ALD-HfO<sub>2</sub> in the anode are etched to form the anode recess structure of the high barrier height Schottky contact (Figure 2(e)). Finally, the evaporation of Ni/Au (50/150 nm) metal stack was carried out to serve as the anode metal and pads after removing the ALD-HfO<sub>2</sub> above the cathode (Figure 2(f)). Measurement suggests that  $V_{TH}$  of the recessed MIS-structure is 0.6 V. Microscopy image of the CA-LFED with  $L_{AC} = 4.5$  μm is shown in Figure 4. The devices with  $L_{AC} = 9.5/19.5$  μm are also realized in the same process for comparison.

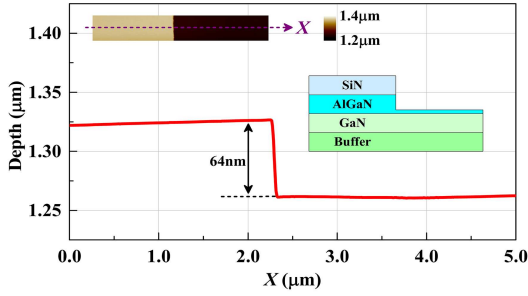


Figure 3 (Color online) AFM morphology after etching the anode in-situ SiN passivation and AlGaN barrier.

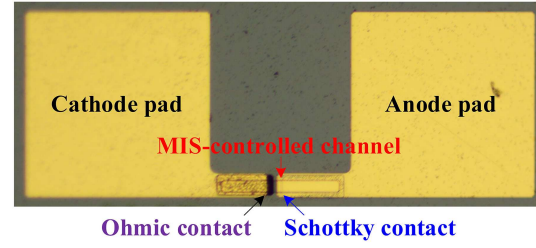


Figure 4 (Color online) Microscopy image of the fabricated CA-LFED with  $L_{AC} = 4.5 \mu\text{m}$ .

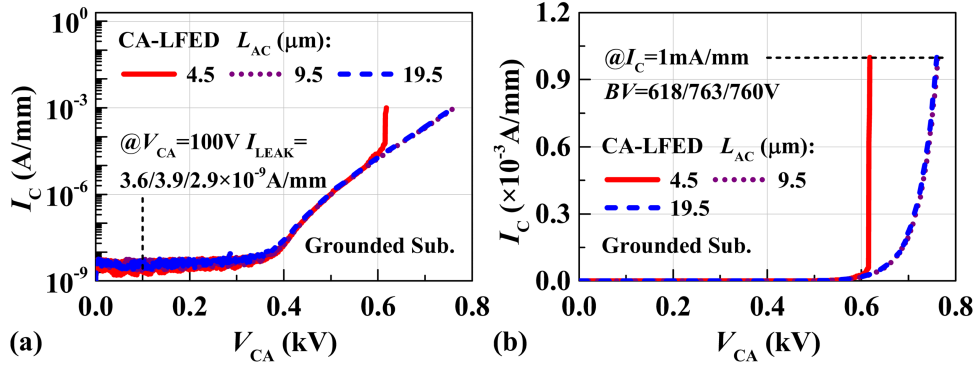


Figure 5 (Color online) (a) Log and (b) linear scale reverse  $I$ - $V$  characteristics of the CA-LFEDs with  $L_{AC} = 4.5/9.5/19.5 \mu\text{m}$ .

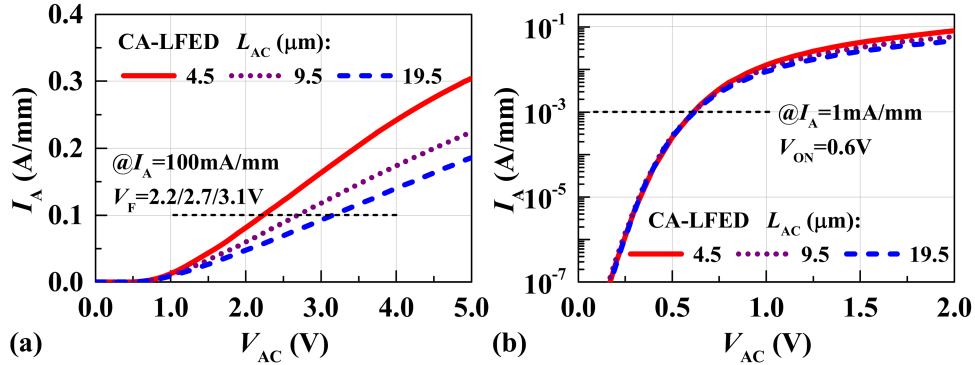
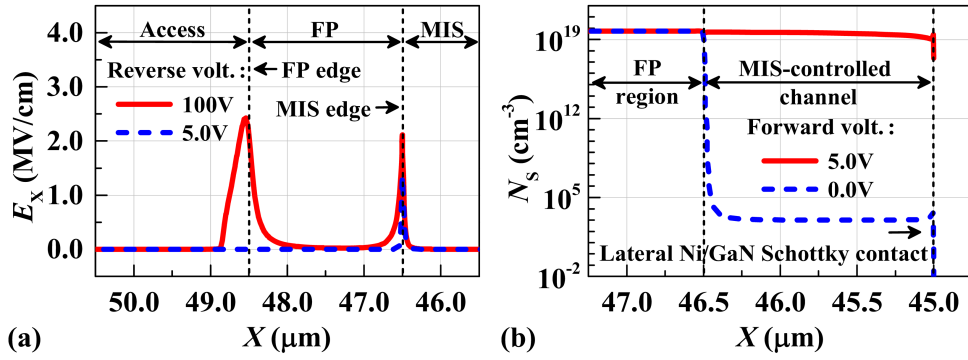


Figure 6 (Color online) (a) Linear and (b) log scale forward  $I$ - $V$  characteristics of the CA-LFEDs with  $L_{AC} = 4.5/9.5/19.5 \mu\text{m}$ .

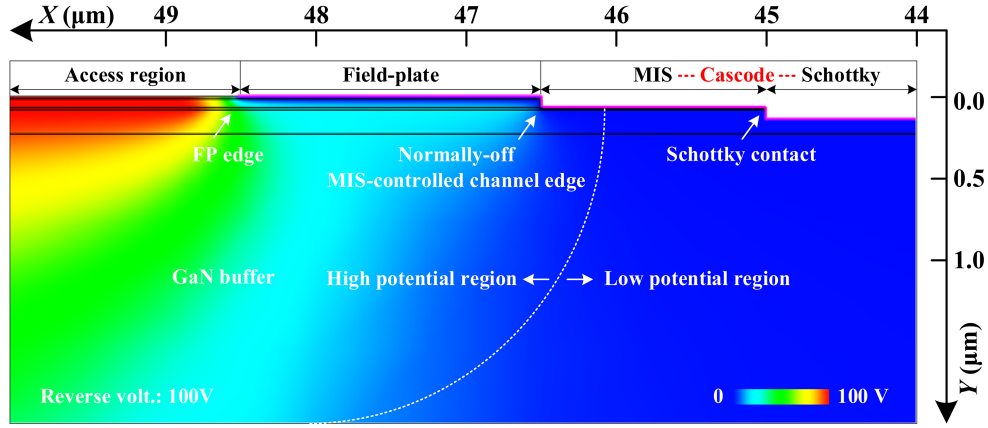
### 3 Results, mechanisms, and discussions

Figure 5 shows reverse  $I$ - $V$  characteristics of the CA-LFEDs with various  $L_{AC}$ .  $V_{CA}$  and  $I_C$  are the cathode-to-anode voltage and cathode current, respectively. Both the normally-off MIS-controlled channel and high barrier height Schottky contact are beneficial to suppress the  $I_{LEAK}$ . It is suggested that the  $I_{LEAK}$  values of the CA-LFEDs maintain as low as  $3.6/3.9/2.9 \times 10^{-9}$  A/mm respectively with various  $L_{AC} = 4.5/9.5/19.5 \mu\text{m}$ , and the devices also obtain high BVs of 618/763/760 V, respectively. Figure 6 presents forward  $I$ - $V$  characteristics of the CA-LFEDs with various  $L_{AC}$ . The  $V_F$  and turn-on voltage ( $V_{ON}$ ) are extracted at the forward current density of 100 and 1 mA/mm, respectively.  $V_{AC}$  and  $I_A$  represent the anode-to-cathode voltage and anode current, respectively. With the increase of  $L_{AC}$ , the  $V_F$  of the CA-LFED rises slightly from 2.2 to 3.1 V, while the  $V_{ON}$  is almost unchanged at 0.6 V. The forward performance indicates that the CA-LFED has an acceptable low  $V_F$ .

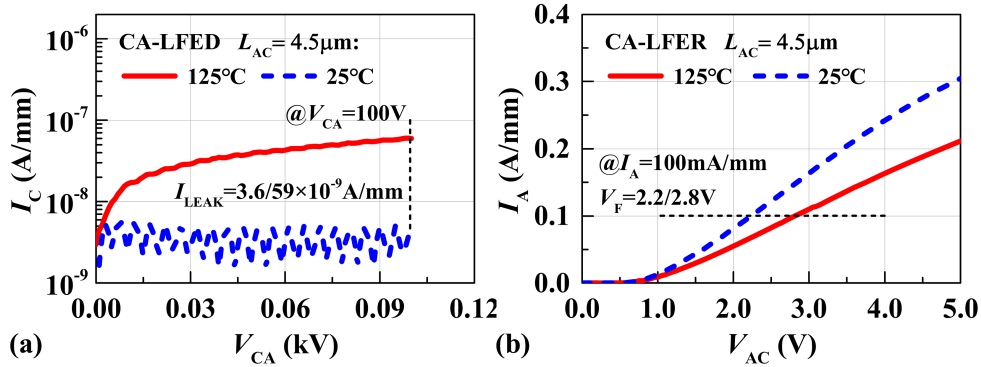
Figure 7 shows the lateral electric-field ( $E_X$ ) and electron concentration ( $N_S$ ) along the 2DEG channel in the CA-LFED. At a reverse voltage of 5 V, the electric-field peak is crowded at the normally-off MIS-



**Figure 7** (Color online) (a) Lateral electric-field ( $E_x$ ) and (b) electron concentration ( $N_s$ ) distributions along the 2DEG channel in the CA-LFED.



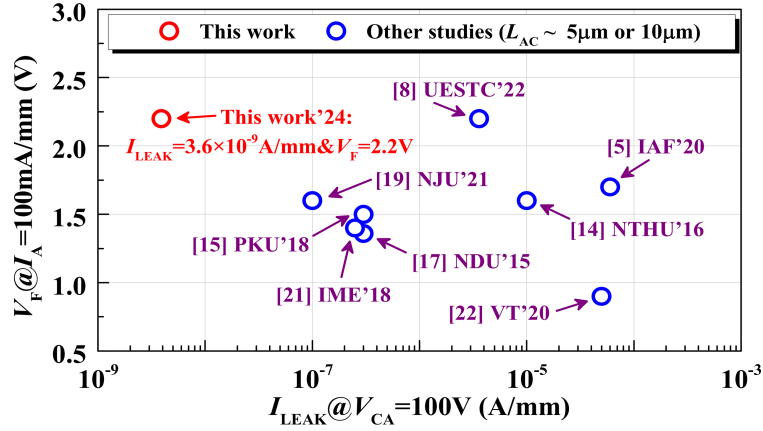
**Figure 8** (Color online) Electrostatic potential distributions at a reverse voltage of 100 V in the CA-LFED.



**Figure 9** (Color online) High temperature (a) reverse and (b) forward  $I$ - $V$  comparisons of the CA-LFEDs with  $L_{AC} = 4.5 \mu\text{m}$ .

controlled channel edge. As reverse bias increases to 100 V, the MIS edge electric-field peak is clamped. A higher electric-field peak emerges at the FP edge, suggesting that the high electric-field is effectively prevented, and the CA-LFED can present an ultralow  $I_{LEAK}$ . When forward voltage rises from 0 to 5 V, the 2DEG concentration of the normally-off MIS-controlled channel is improved to the same level as that under the FP region, indicating that the CA-LFED has a relatively low  $V_F$ . Figure 8 shows the electrostatic potential distribution at a reverse voltage of 100 V in the CA-LFED. The high potential region is located at the access region and prevented by the normally-off MIS-controlled channel and FP. This protects the Schottky contact from high reverse potential and makes the device have low  $I_{LEAK}$ . Feasibility of the simulation parameters and models has been confirmed in our previous studies [24–26].

Figure 9 shows the high temperature reverse and forward  $I$ - $V$  comparisons of the CA-LFED with  $L_{AC} = 4.5 \mu\text{m}$ . The characteristics with 125°C are measured in a high temperature device test system with



**Figure 10** (Color online)  $V_F$ - $I_{LEAK}$  comparisons of the CA-LFED and state-of-the-art devices ( $L_{AC}$  about 5 or 10  $\mu\text{m}$ ).

**Table 2** Comparisons about the reverse leakage current and forward conduction current densities.

Ref.	Reverse leakage current (A/mm) (at $V_{CA} = 100$ V)	Forward conduction current (A/mm) (at $V_{AC} = 3$ V)
IAF'20 [5]	$6.0 \times 10^{-5}$	0.20
UESTC'22 [8]	$3.6 \times 10^{-6}$	0.14
NTHU'16 [14]	$1.0 \times 10^{-5}$	0.17
PKU'18 [15]	$2.5 \times 10^{-7}$	0.40
NDU'15 [17]	$3.0 \times 10^{-7}$	0.28
NJU'21 [19]	$1.0 \times 10^{-7}$	0.37
IME'18 [21]	$3.0 \times 10^{-7}$	0.15
VT'20 [22]	$5.0 \times 10^{-5}$	0.87
This work'24	$3.6 \times 10^{-9}$	0.16

a maximum voltage of 100 V. As temperature rises from 25°C to 125°C, the  $I_{LEAK}$  in the CA-LFED increases about 16 times from  $3.6 \times 10^{-9}$  to  $59 \times 10^{-9}$  A/mm, and the  $V_F$  of the device is changed from 2.2 to 2.8 V. The  $V_F$  and  $I_{LEAK}$  at 125°C suggest that the CA-LFED exhibits excellent high temperature stability.

Figure 10 shows the  $V_F$ - $I_{LEAK}$  comparisons of the CA-LFED and several state-of-the-art devices ( $L_{AC}$  about 5 or 10  $\mu\text{m}$ ). Table 2 compares this work with other lateral GaN-based diodes about the reverse leakage current and forward conduction current densities. An ultralow  $I_{LEAK} = 3.6 \times 10^{-9}$  A/mm and a relatively low  $V_F = 2.2$  V are obtained in the CA-LFED, verifying the ultralow leakage current of the device and suggesting the competitive  $V_F$ - $I_{LEAK}$  trade-off among the existing studies. Additionally, compared to the standard p-GaN gate HEMT in the third quadrant [27], the CA-LFED achieves the similar  $I_{LEAK}$  as well as the lower  $V_F$ , although it has a relatively complex anode structure (pros and cons).

## 4 Conclusion

In this work, we propose an ultralow  $I_{LEAK}$  CA-LFED based on AlGaIn/GaN HEMT. The cascoded normally-off MIS-controlled channel and high barrier height Schottky contact contribute to significantly suppressing the  $I_{LEAK}$  and meanwhile ensuring relatively low  $V_F$ . Verified by the device fabrication, the CA-LFED shows an ultralow  $I_{LEAK}$  of  $3.6 \times 10^{-9}$  A/mm, a relatively low  $V_F$  of 2.2 V, and a high BV > 600 V. The performance suggests that the CA-LFED can be a competitive candidate for the GaN power diode applications demanding for ultralow  $I_{LEAK}$  and a better  $V_F$ - $I_{LEAK}$  trade-off.

**Acknowledgements** This work was supported in part by National Natural Science Foundation of China (Grant No. 62334003) and Guangdong Basic and Applied Basic Research Foundation (Grant No. 2020A1515110567). Zeheng WANG declares that his contribution to this research was conducted without any funding or involvement from the aforementioned funding sources.

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**Funding** Open access funding provided by CSIRO Library Services.

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