

• Supplementary File •

What is the optimal inter-site distance in multi-BS cooperative sensing?

Zhichu Ren¹, Yiming Yu², Hong Ren^{1*}, Cunhua Pan^{1*} & Jiangzhou Wang¹

¹National Mobile Communications Research Laboratory, Southeast University, Nanjing 211189, China;

²China Mobile Group Design Institute Co., Ltd., Beijing 100080, China

Appendix A Derivation of the radar SINR

According to [1], the radar SINRs of BS₁ and BS₂ can be respectively expressed as

$$\text{SINR}_1 = \text{Tr}(|a_1|^2 \mathbf{A}_1(\theta_1, \phi_1) \mathbf{w}_1 \mathbf{w}_1^H \mathbf{A}_1^H(\theta_1, \phi_1) (\rho |b_{1,2}|^2 \mathbf{G}_{1,2}(\theta_1, \phi_1, \theta_2, \phi_2) \mathbf{w}_2 \mathbf{w}_2^H \mathbf{G}_{1,2}^H(\theta_1, \phi_1, \theta_2, \phi_2) + \sigma^2 \mathbf{I}_{N_r})^{-1}), \quad (\text{A1})$$

$$\text{SINR}_2 = \text{Tr}(|a_2|^2 \mathbf{A}_2(\theta_2, \phi_2) \mathbf{w}_2 \mathbf{w}_2^H \mathbf{A}_2^H(\theta_2, \phi_2) (\rho |b_{2,1}|^2 \mathbf{G}_{2,1}(\theta_2, \phi_2, \theta_1, \phi_1) \mathbf{w}_1 \mathbf{w}_1^H \mathbf{G}_{2,1}^H(\theta_2, \phi_2, \theta_1, \phi_1) + \sigma^2 \mathbf{I}_{N_r})^{-1}). \quad (\text{A2})$$

By adopting MRT precoding and using the equation $\mathbf{a}_t^H(\theta_1, \phi_1) \mathbf{a}_t(\theta_1, \phi_1) = \mathbf{a}_t^H(\theta_2, \phi_2) \mathbf{a}_t(\theta_2, \phi_2) = \frac{N_t x \times N_t z}{N_t} = 1$, the radar SINRs can be further expressed as

$$\text{SINR}_1 = \text{Tr}(|a_1|^2 P_1 \mathbf{A}_{r,1} (\rho P_2 |b_{1,2}|^2 \mathbf{A}_{r,1} + \sigma^2 \mathbf{I}_{N_r})^{-1}), \quad (\text{A3})$$

$$\text{SINR}_2 = \text{Tr}(|a_2|^2 P_2 \mathbf{A}_{r,2} (\rho P_1 |b_{2,1}|^2 \mathbf{A}_{r,2} + \sigma^2 \mathbf{I}_{N_r})^{-1}), \quad (\text{A4})$$

where $\mathbf{A}_{r,1} = \mathbf{a}_r(\theta_1, \phi_1) \mathbf{a}_r^H(\theta_1, \phi_1)$ and $\mathbf{A}_{r,2} = \mathbf{a}_r(\theta_2, \phi_2) \mathbf{a}_r^H(\theta_2, \phi_2)$ are both rank-1 matrices. Consider the eigenvalue decomposition of $\mathbf{A}_{r,1}$ and $\mathbf{A}_{r,2}$ for $\mathbf{A}_{r,1} = \mathbf{U}_1^H \mathbf{A}_1 \mathbf{U}_1$ and $\mathbf{A}_{r,2} = \mathbf{U}_2^H \mathbf{A}_2 \mathbf{U}_2$, which satisfy $\mathbf{U}_1^H \mathbf{U}_1 = \mathbf{U}_2^H \mathbf{U}_2 = \mathbf{I}_{N_r}$ and $\mathbf{A}_1 = \mathbf{A}_2 = \text{diag}\{1, 0, \dots, 0\}$. The expressions of SINR_1 and SINR_2 can be further calculated as

$$\begin{aligned} \text{SINR}_1 &= \text{Tr}(|a_1|^2 P_1 \mathbf{A}_{r,1} (\rho P_2 |b_{1,2}|^2 \mathbf{A}_{r,1} + \sigma^2 \mathbf{I}_{N_r})^{-1}) = \text{Tr}(|a_1|^2 P_1 \mathbf{U}_1^H \mathbf{A}_1 \mathbf{U}_1 (\rho P_2 |b_{1,2}|^2 \mathbf{U}_1^H \mathbf{A}_1 \mathbf{U}_1 + \sigma^2 \mathbf{U}_1^H \mathbf{U}_1)^{-1}) \\ &= \text{Tr}(|a_1|^2 P_1 \mathbf{U}_1^H \mathbf{A}_1 \mathbf{U}_1 \mathbf{U}_1^{-1} (\rho P_2 |b_{1,2}|^2 \mathbf{A}_1 + \sigma^2 \mathbf{I}_{N_r})^{-1} (\mathbf{U}_1^{-1})^H) = |a_1|^2 P_1 \text{Tr}(\mathbf{A}_1 (\rho P_2 |b_{1,2}|^2 \mathbf{A}_1 + \sigma^2 \mathbf{I}_{N_r})^{-1}), \end{aligned} \quad (\text{A5})$$

$$\begin{aligned} \text{SINR}_2 &= \text{Tr}(|a_2|^2 P_2 \mathbf{A}_{r,2} (\rho P_1 |b_{2,1}|^2 \mathbf{A}_{r,2} + \sigma^2 \mathbf{I}_{N_r})^{-1}) = \text{Tr}(|a_2|^2 P_2 \mathbf{U}_2^H \mathbf{A}_2 \mathbf{U}_2 (\rho P_1 |b_{2,1}|^2 \mathbf{U}_2^H \mathbf{A}_2 \mathbf{U}_2 + \sigma^2 \mathbf{U}_2^H \mathbf{U}_2)^{-1}) \\ &= \text{Tr}(|a_2|^2 P_2 \mathbf{U}_2^H \mathbf{A}_2 \mathbf{U}_2 \mathbf{U}_2^{-1} (\rho P_1 |b_{2,1}|^2 \mathbf{A}_2 + \sigma^2 \mathbf{I}_{N_r})^{-1} (\mathbf{U}_2^{-1})^H) = |a_2|^2 P_2 \text{Tr}(\mathbf{A}_2 (\rho P_1 |b_{2,1}|^2 \mathbf{A}_2 + \sigma^2 \mathbf{I}_{N_r})^{-1}). \end{aligned} \quad (\text{A6})$$

Note that

$$\mathbf{A}_1 (\rho P_2 |b_{1,2}|^2 \mathbf{A}_1 + \sigma^2 \mathbf{I}_{N_r})^{-1} = \begin{bmatrix} 1 & 0 & \dots & 0 \\ 0 & 0 & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \dots & 0 \end{bmatrix} \begin{bmatrix} \rho P_2 |b_{1,2}|^2 + \sigma^2 & 0 & \dots & 0 \\ 0 & \sigma^2 & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \dots & \sigma^2 \end{bmatrix}^{-1} = \begin{bmatrix} \frac{1}{\rho P_2 |b_{1,2}|^2 + \sigma^2} & 0 & \dots & 0 \\ 0 & 0 & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \dots & 0 \end{bmatrix}, \quad (\text{A7})$$

$$\mathbf{A}_2 (\rho P_1 |b_{2,1}|^2 \mathbf{A}_2 + \sigma^2 \mathbf{I}_{N_r})^{-1} = \begin{bmatrix} 1 & 0 & \dots & 0 \\ 0 & 0 & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \dots & 0 \end{bmatrix} \begin{bmatrix} \rho P_1 |b_{2,1}|^2 + \sigma^2 & 0 & \dots & 0 \\ 0 & \sigma^2 & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \dots & \sigma^2 \end{bmatrix}^{-1} = \begin{bmatrix} \frac{1}{\rho P_1 |b_{2,1}|^2 + \sigma^2} & 0 & \dots & 0 \\ 0 & 0 & \dots & 0 \\ \vdots & \vdots & \ddots & \vdots \\ 0 & 0 & \dots & 0 \end{bmatrix}. \quad (\text{A8})$$

Finally, we derive the expressions of the radar SINR when the UAV is located at (x, y, z) as follows

$$\text{SINR}_1(x, y, z) = \frac{P_1 |a_1|^2}{\rho P_2 |b_{1,2}|^2 + \sigma^2} = \frac{\frac{GCP_1}{(x^2 + y^2 + (z - h_{\text{BS}})^2)^2}}{\frac{\rho GCP_2}{(x^2 + (d-y)^2 + (z - h_{\text{BS}})^2)(x^2 + y^2 + (z - h_{\text{BS}})^2)} + \sigma^2}, \quad (\text{A9})$$

$$\text{SINR}_2(x, y, z) = \frac{P_2 |a_2|^2}{\rho P_1 |b_{2,1}|^2 + \sigma^2} = \frac{\frac{GCP_2}{(x^2 + (d-y)^2 + (z - h_{\text{BS}})^2)^2}}{\frac{\rho GCP_1}{(x^2 + (d-y)^2 + (z - h_{\text{BS}})^2)(x^2 + y^2 + (z - h_{\text{BS}})^2)} + \sigma^2}. \quad (\text{A10})$$

* Corresponding author (email: hren@seu.edu.cn, cpan@seu.edu.cn)

To evaluate the sensing performance statistically, the UAV is assumed to obey uniform distribution in the cuboid region $\mathcal{D} = [-x_0, x_0] \times [\alpha d, \beta d] \times [h_{\min}, h_{\max}]$. Therefore, the probability density function (PDF) of the location of the UAV can be expressed as follows

$$f(x, y, z) = \begin{cases} \frac{1}{V_{\mathcal{D}}}, & (x, y, z) \in \mathcal{D} \\ 0, & (x, y, z) \notin \mathcal{D} \end{cases} \quad (\text{A11})$$

where $V_{\mathcal{D}}$ denotes the volume of \mathcal{D} . The expectations of SINR_1 and SINR_2 are calculated as follows

$$\begin{aligned} \overline{\text{SINR}_1} &= \mathbb{E}\{\text{SINR}_1(x, y, z)\} = \frac{1}{V_{\mathcal{D}}} \iiint_{\mathcal{D}} \text{SINR}_1(x, y, z) dx dy dz \\ &= \frac{1}{(\beta - \alpha)x_0(h_{\max} - h_{\min})d} \int_{\alpha d}^{\beta d} dy \int_0^{x_0} dx \int_{h_{\min}}^{h_{\max}} \frac{\frac{GCP_1}{(x^2+y^2+(z-h_{\text{BS}})^2)^2}}{\frac{\rho GCP_2}{(x^2+(d-y)^2+(z-h_{\text{BS}})^2)(x^2+y^2+(z-h_{\text{BS}})^2)} + \sigma^2} dz, \end{aligned} \quad (\text{A12})$$

$$\begin{aligned} \overline{\text{SINR}_2} &= \mathbb{E}\{\text{SINR}_2(x, y, z)\} = \frac{1}{V_{\mathcal{D}}} \iiint_{\mathcal{D}} \text{SINR}_2(x, y, z) dx dy dz \\ &= \frac{1}{(\beta - \alpha)x_0(h_{\max} - h_{\min})d} \int_{\alpha d}^{\beta d} dy \int_0^{x_0} dx \int_{h_{\min}}^{h_{\max}} \frac{\frac{GCP_2}{(x^2+(d-y)^2+(z-h_{\text{BS}})^2)^2}}{\frac{\rho GCP_1}{(x^2+(d-y)^2+(z-h_{\text{BS}})^2)(x^2+y^2+(z-h_{\text{BS}})^2)} + \sigma^2} dz. \end{aligned} \quad (\text{A13})$$

Due to symmetry, we only consider the case where the UAV is closer to BS_1 , i.e., $\alpha < \beta \leq 0.5$. Consequently, we have $\overline{\text{SINR}} = \max\{\overline{\text{SINR}_1}, \overline{\text{SINR}_2}\} = \overline{\text{SINR}_1}$. It is worth noting that the above integrals cannot be solved analytically, so we use numerical methods to calculate the above integrals.

Appendix B Derivation of the joint detection probability

We consider the likelihood ratio test (LRT) detector over one sensing block of L symbols. For BS_1 , the detection problem can be formulated as a binary hypothesis testing problem [2] as follows

$$\begin{cases} \mathbf{Y}_{1,2} = \mathbf{N}, & \mathcal{H}_0 \\ \mathbf{Y}_{1,2} = a_1 \mathbf{A}_1(\theta_1, \phi_1) \mathbf{w}_1 \mathbf{s}_1 + \sqrt{\rho} b_{1,2} \mathbf{G}_{1,2}(\theta_1, \phi_1, \theta_2, \phi_2) \mathbf{w}_2 \mathbf{s}_2 + \mathbf{N}, & \mathcal{H}_1 \end{cases} \quad (\text{B1})$$

where $\mathbf{Y}_{1,2} = [\mathbf{y}_{1,2}(1), \dots, \mathbf{y}_{1,2}(L)]$, $\mathbf{N} = [\mathbf{n}(1), \dots, \mathbf{n}(L)]$, $\mathbf{s}_1 = [s_{1,1}, \dots, s_{1,L}]$, and $\mathbf{s}_2 = [s_{2,1}, \dots, s_{2,L}]$. In the mono-static architecture, $\sqrt{\rho} b_{1,2} \mathbf{G}_{1,2}(\theta_1, \phi_1, \theta_2, \phi_2) \mathbf{w}_2 \mathbf{s}_2$ and \mathbf{N} are regarded as interference/noise for BS_1 . After signal vectorization, the problem can be further expressed as

$$\begin{cases} \tilde{\mathbf{y}}_1 = -\mathbf{u}_2 + \mathbf{n}_s, & \mathcal{H}_0 \\ \tilde{\mathbf{y}}_1 = \mathbf{u}_1 + \mathbf{n}_s, & \mathcal{H}_1 \end{cases} \quad (\text{B2})$$

where $\tilde{\mathbf{y}}_1 = \text{vec}\{\mathbf{Y}_{1,2}\}$, $\mathbf{u}_1 = \text{vec}\{a_1 \mathbf{A}_1(\theta_1, \phi_1) \mathbf{w}_1 \mathbf{s}_1\}$, $\mathbf{u}_2 = \text{vec}\{\sqrt{\rho} b_{1,2} \mathbf{G}_{1,2}(\theta_1, \phi_1, \theta_2, \phi_2) \mathbf{w}_2 \mathbf{s}_2\}$, $\mathbf{n}_s = \text{vec}\{\sqrt{\rho} b_{1,2} \mathbf{G}_{1,2}(\theta_1, \phi_1, \theta_2, \phi_2) \mathbf{w}_2 \mathbf{s}_2 + \mathbf{N}\} \sim \mathcal{CN}(\mathbf{0}, \mathbf{R})$, and $\mathbf{R} = \mathbf{I}_L \otimes (\rho |b_{1,2}|^2 \mathbf{G}_{1,2}^H(\theta_1, \phi_1, \theta_2, \phi_2) \mathbf{w}_2 \mathbf{w}_2^H \mathbf{G}_{1,2}(\theta_1, \phi_1, \theta_2, \phi_2) + \sigma^2 \mathbf{I}_{N_r}) \triangleq \mathbf{I}_L \otimes \tilde{\mathbf{R}}$. Therefore, the LRT detector can be expressed as

$$\Lambda(\tilde{\mathbf{y}}_1) = \frac{f(\tilde{\mathbf{y}}_1 | \mathcal{H}_1)}{f(\tilde{\mathbf{y}}_1 | \mathcal{H}_0)} \underset{\mathcal{H}_0}{\overset{\mathcal{H}_1}{\geq}} \kappa, \quad (\text{B3})$$

where κ is a certain threshold which is determined according to a target value of probability of false alarm P_{FA} (the probability that the system still determines the presence of a target when only noise/interference is present) for performing constant false alarm rate (CFAR) detection [3]. $f(\tilde{\mathbf{y}}_1 | \mathcal{H}_1)$ and $f(\tilde{\mathbf{y}}_1 | \mathcal{H}_0)$ denote the PDFs of $\tilde{\mathbf{y}}_1$ under the hypotheses \mathcal{H}_1 and \mathcal{H}_0 , respectively, which can be expressed as

$$f(\tilde{\mathbf{y}}_1 | \mathcal{H}_0) = \frac{1}{\pi^{N_r L} \det(\mathbf{R})} \exp(-(\tilde{\mathbf{y}}_1 + \mathbf{u}_2)^H \mathbf{R}^{-1} (\tilde{\mathbf{y}}_1 + \mathbf{u}_2)), \quad (\text{B4})$$

$$f(\tilde{\mathbf{y}}_1 | \mathcal{H}_1) = \frac{1}{\pi^{N_r L} \det(\mathbf{R})} \exp(-(\tilde{\mathbf{y}}_1 - \mathbf{u}_1)^H \mathbf{R}^{-1} (\tilde{\mathbf{y}}_1 - \mathbf{u}_1)). \quad (\text{B5})$$

After taking the logarithmic operation, the logarithmic LRT function can be expressed as

$$\ln \Lambda(\tilde{\mathbf{y}}_1) = (\tilde{\mathbf{y}}_1 + \mathbf{u}_2)^H \mathbf{R}^{-1} (\tilde{\mathbf{y}}_1 + \mathbf{u}_2) - (\tilde{\mathbf{y}}_1 - \mathbf{u}_1)^H \mathbf{R}^{-1} (\tilde{\mathbf{y}}_1 - \mathbf{u}_1). \quad (\text{B6})$$

$\ln \Lambda(\tilde{\mathbf{y}}_1)$ under hypotheses \mathcal{H}_0 and \mathcal{H}_1 , respectively, are distributed as

$$\begin{cases} \ln \Lambda(\tilde{\mathbf{y}}_1) \sim \mathcal{N}(-\mathbf{u}_1^H \mathbf{R}^{-1} \mathbf{u}_2 - \mathbf{u}_2^H \mathbf{R}^{-1} \mathbf{u}_1 - \mathbf{u}_1^H \mathbf{R}^{-1} \mathbf{u}_1 - \mathbf{u}_2^H \mathbf{R}^{-1} \mathbf{u}_2, 2\mathbf{u}_1^H \mathbf{R}^{-1} \mathbf{u}_1 + 2\mathbf{u}_2^H \mathbf{R}^{-1} \mathbf{u}_2), & \mathcal{H}_0 \\ \ln \Lambda(\tilde{\mathbf{y}}_1) \sim \mathcal{N}(\mathbf{u}_1^H \mathbf{R}^{-1} \mathbf{u}_2 + \mathbf{u}_2^H \mathbf{R}^{-1} \mathbf{u}_1 + \mathbf{u}_1^H \mathbf{R}^{-1} \mathbf{u}_1 + \mathbf{u}_2^H \mathbf{R}^{-1} \mathbf{u}_2, 2\mathbf{u}_1^H \mathbf{R}^{-1} \mathbf{u}_1 + 2\mathbf{u}_2^H \mathbf{R}^{-1} \mathbf{u}_2), & \mathcal{H}_1 \end{cases} \quad (\text{B7})$$

Therefore, the probability of false alarm P_{FA} and detection probability of BS_1 interfered with by BS_2 (the probability that the system correctly detects the target in the presence of noise and interference) can be respectively expressed as

$$P_{\text{FA}} = \Pr\{\ln \Lambda(\tilde{\mathbf{y}}_1) \geq \ln \kappa | \mathcal{H}_0\} = Q\left(\frac{\ln \kappa + \mathbf{u}_1^H \mathbf{R}^{-1} \mathbf{u}_2 + \mathbf{u}_2^H \mathbf{R}^{-1} \mathbf{u}_1 + \mathbf{u}_1^H \mathbf{R}^{-1} \mathbf{u}_1 + \mathbf{u}_2^H \mathbf{R}^{-1} \mathbf{u}_2}{\sqrt{2(\mathbf{u}_1^H \mathbf{R}^{-1} \mathbf{u}_1 + \mathbf{u}_2^H \mathbf{R}^{-1} \mathbf{u}_2)}}\right), \quad (\text{B8})$$

$$P_{1,2} = \Pr\{\ln \Lambda(\tilde{\mathbf{y}}_1) \geq \ln \kappa | \mathcal{H}_1\} = Q\left(\frac{\ln \kappa - \mathbf{u}_1^H \mathbf{R}^{-1} \mathbf{u}_2 - \mathbf{u}_2^H \mathbf{R}^{-1} \mathbf{u}_1 - \mathbf{u}_1^H \mathbf{R}^{-1} \mathbf{u}_1 - \mathbf{u}_2^H \mathbf{R}^{-1} \mathbf{u}_2}{\sqrt{2(\mathbf{u}_1^H \mathbf{R}^{-1} \mathbf{u}_1 + \mathbf{u}_2^H \mathbf{R}^{-1} \mathbf{u}_2)}}\right), \quad (\text{B9})$$

where $Q(x) = \frac{1}{\sqrt{2\pi}} \int_x^\infty e^{-\frac{t^2}{2}} dt$ denotes the Q-function and the detection threshold κ can be determined by

$$\ln \kappa = Q^{-1}(P_{\text{FA}}) \sqrt{2(\mathbf{u}_1^H \mathbf{R}^{-1} \mathbf{u}_1 + \mathbf{u}_2^H \mathbf{R}^{-1} \mathbf{u}_2)} - \mathbf{u}_1^H \mathbf{R}^{-1} \mathbf{u}_2 - \mathbf{u}_2^H \mathbf{R}^{-1} \mathbf{u}_1 - \mathbf{u}_1^H \mathbf{R}^{-1} \mathbf{u}_1 - \mathbf{u}_2^H \mathbf{R}^{-1} \mathbf{u}_2, \quad (\text{B10})$$

where $Q^{-1}(x)$ denotes the inverse Q-function. By defining $\kappa = Q^{-1}(P_{\text{FA}})$, the detection probability of BS₁ can be further expressed as

$$P_{1,2} = Q\left(\kappa - \frac{2\mathbf{u}_2^H \mathbf{R}^{-1} \mathbf{u}_1 + 2\mathbf{u}_1^H \mathbf{R}^{-1} \mathbf{u}_2 + 2\mathbf{u}_1^H \mathbf{R}^{-1} \mathbf{u}_1 + 2\mathbf{u}_2^H \mathbf{R}^{-1} \mathbf{u}_2}{\sqrt{2(\mathbf{u}_1^H \mathbf{R}^{-1} \mathbf{u}_1 + \mathbf{u}_2^H \mathbf{R}^{-1} \mathbf{u}_2)}}\right). \quad (\text{B11})$$

By using the transformation $\text{Tr}(\mathbf{ABCD}) = \text{vec}^H\{\mathbf{D}^H\}(\mathbf{C}^T \otimes \mathbf{A})\text{vec}\{\mathbf{B}\}$ and the assumption that $\mathbf{s}_1^H \mathbf{s}_2 \approx \mathbb{E}\{\mathbf{s}_1^H \mathbf{s}_2\} = 0$, $\mathbf{s}_2^H \mathbf{s}_1 \approx \mathbb{E}\{\mathbf{s}_2^H \mathbf{s}_1\} = 0$, $\mathbf{s}_1^H \mathbf{s}_1 \approx \mathbb{E}\{\mathbf{s}_1^H \mathbf{s}_1\} = L$ and $\mathbf{s}_2^H \mathbf{s}_2 \approx \mathbb{E}\{\mathbf{s}_2^H \mathbf{s}_2\} = L$, we can rewrite P_1 when the UAV is located at (x, y, z) into a more intractable form as follows

$$P_{1,2}(x, y, z) = Q\left(\kappa - \sqrt{2L(\text{SINR}_1(x, y, z) + \frac{\rho P_2 |b_{1,2}|^2}{\rho P_2 |b_{1,2}|^2 + \sigma^2})}\right). \quad (\text{B12})$$

By adopting the similar derivation, the detection probability of BS₂ interfered with by BS₁ when the UAV is located at (x, y, z) can be expressed as

$$P_{2,1}(x, y, z) = Q\left(\kappa - \sqrt{2L(\text{SINR}_2(x, y, z) + \frac{\rho P_1 |b_{2,1}|^2}{\rho P_1 |b_{2,1}|^2 + \sigma^2})}\right). \quad (\text{B13})$$

Eventually, according to the equation $1 - Q(x) = Q(-x)$, the joint detection probability of the two BSs when the UAV is located at (x, y, z) can be calculated as

$$\begin{aligned} P_{\text{D}}(x, y, z) &= 1 - (1 - P_{1,2}(x, y, z)) \cdot (1 - P_{2,1}(x, y, z)) \\ &= 1 - Q\left(\sqrt{2L(\text{SINR}_1(x, y, z) + \frac{\rho P_2 |b_{1,2}|^2}{\rho P_2 |b_{1,2}|^2 + \sigma^2})} - \kappa\right) \cdot Q\left(\sqrt{2L(\text{SINR}_2(x, y, z) + \frac{\rho P_1 |b_{2,1}|^2}{\rho P_1 |b_{2,1}|^2 + \sigma^2})} - \kappa\right). \end{aligned} \quad (\text{B14})$$

Similarly, the expectation of the joint detection probability is calculated as follows

$$\begin{aligned} \overline{P_{\text{D}}} &= \mathbb{E}\{P_{\text{D}}(x, y, z)\} = \frac{1}{V_{\text{D}}} \iiint_{\text{D}} P_{\text{D}}(x, y, z) dx dy dz \\ &= \frac{1}{(\beta - \alpha)x_0(h_{\text{max}} - h_{\text{min}})d} \int_{\alpha d}^{\beta d} dy \int_0^{x_0} dx \int_{h_{\text{min}}}^{h_{\text{max}}} P_{\text{D}}(x, y, z) dz. \end{aligned} \quad (\text{B15})$$

It is worth noting that the above integral cannot be solved analytically, so we use numerical methods to calculate the above integral.

Appendix C Derivation of partial derivatives of the average radar SINR and the average joint detection probability with respect to inter-site distance d

Firstly, the partial derivatives of $\text{SINR}_1(x, y, z)$ and $\text{SINR}_2(x, y, z)$ with respect to inter-site distance d are calculated as follows

$$\begin{aligned} \frac{\partial \text{SINR}_1(x, y, z)}{\partial d} &= \frac{-2B_1(d-y)(x^2 + (d-y)^2 + (z-h_{\text{BS}})^2)(x^2 + y^2 + (z-h_{\text{BS}})^2)^2}{(A_1(x^2 + y^2 + (z-h_{\text{BS}})^2) + B_1(x^2 + y^2 + (z-h_{\text{BS}})^2)^2(x^2 + (d-y)^2 + (z-h_{\text{BS}})^2))^2} \\ &\quad + \frac{2(d-y)}{A_1(x^2 + y^2 + (z-h_{\text{BS}})^2) + B_1(x^2 + y^2 + (z-h_{\text{BS}})^2)^2(x^2 + (d-y)^2 + (z-h_{\text{BS}})^2)}, \end{aligned} \quad (\text{C1})$$

$$\frac{\partial \text{SINR}_2(x, y, z)}{\partial d} = \frac{-(x^2 + y^2 + (z-h_{\text{BS}})^2)(2A_2(d-y) + 4B_2(d-y)(x^2 + y^2 + (z-h_{\text{BS}})^2)(x^2 + (d-y)^2 + (z-h_{\text{BS}})^2))}{(A_2(x^2 + (d-y)^2 + (z-h_{\text{BS}})^2) + B_2(x^2 + (d-y)^2 + (z-h_{\text{BS}})^2)^2(x^2 + y^2 + (z-h_{\text{BS}})^2))^2}, \quad (\text{C2})$$

where $A_1 = \frac{\rho P_2}{P_1}$, $B_1 = \frac{\sigma^2}{GC P_1}$, $A_2 = \frac{\rho P_1}{P_2}$ and $B_2 = \frac{\sigma^2}{GC P_2}$.

Then, by using the derivation formula for integrals with parameters, the partial derivatives of the average radar SINR with respect to the inter-site distance d can be expressed as

$$\begin{aligned} \frac{\partial \overline{\text{SINR}_1}}{\partial d} &= \frac{1}{(\beta - \alpha)x_0(h_{\text{max}} - h_{\text{min}})} \frac{\partial \int_{\alpha d}^{\beta d} dy \int_0^{x_0} dx \int_{h_{\text{min}}}^{h_{\text{max}}} \frac{1}{d} \text{SINR}_1(x, y, z) dz}{\partial d} \\ &= \frac{1}{(\beta - \alpha)x_0(h_{\text{max}} - h_{\text{min}})} \int_{\alpha d}^{\beta d} dy \int_0^{x_0} dx \int_{h_{\text{min}}}^{h_{\text{max}}} \left(-\frac{1}{d^2} \text{SINR}_1(x, y, z) + \frac{1}{d} \frac{\partial \text{SINR}_1(x, y, z)}{\partial d}\right) dz \\ &\quad + \frac{\beta}{(\beta - \alpha)x_0(h_{\text{max}} - h_{\text{min}})} \int_0^{x_0} dx \int_{h_{\text{min}}}^{h_{\text{max}}} \frac{1}{d} \text{SINR}_1(x, \beta d, z) dz - \frac{\alpha}{(\beta - \alpha)x_0(h_{\text{max}} - h_{\text{min}})} \int_0^{x_0} dx \int_{h_{\text{min}}}^{h_{\text{max}}} \frac{1}{d} \text{SINR}_1(x, \alpha d, z) dz, \end{aligned} \quad (\text{C3})$$

$$\begin{aligned} \frac{\partial \overline{\text{SINR}_2}}{\partial d} &= \frac{1}{(\beta - \alpha)x_0(h_{\text{max}} - h_{\text{min}})} \frac{\partial \int_{\alpha d}^{\beta d} dy \int_0^{x_0} dx \int_{h_{\text{min}}}^{h_{\text{max}}} \frac{1}{d} \text{SINR}_2(x, y, z) dz}{\partial d} \\ &= \frac{1}{(\beta - \alpha)x_0(h_{\text{max}} - h_{\text{min}})} \int_{\alpha d}^{\beta d} dy \int_0^{x_0} dx \int_{h_{\text{min}}}^{h_{\text{max}}} \left(-\frac{1}{d^2} \text{SINR}_2(x, y, z) + \frac{1}{d} \frac{\partial \text{SINR}_2(x, y, z)}{\partial d}\right) dz \\ &\quad + \frac{\beta}{(\beta - \alpha)x_0(h_{\text{max}} - h_{\text{min}})} \int_0^{x_0} dx \int_{h_{\text{min}}}^{h_{\text{max}}} \frac{1}{d} \text{SINR}_2(x, \beta d, z) dz - \frac{\alpha}{(\beta - \alpha)x_0(h_{\text{max}} - h_{\text{min}})} \int_0^{x_0} dx \int_{h_{\text{min}}}^{h_{\text{max}}} \frac{1}{d} \text{SINR}_2(x, \alpha d, z) dz. \end{aligned} \quad (\text{C4})$$

Due to symmetry, we only consider the case where the UAV is closer to BS₁, i.e., $\alpha < \beta \leq 0.5$. Consequently, we have $\frac{\partial \overline{\text{SINR}}}{\partial d} = \frac{\partial (\max\{\text{SINR}_1, \text{SINR}_2\})}{\partial d} = \frac{\partial \text{SINR}_1}{\partial d}$.

By defining

$$D_1 \triangleq \frac{\rho P_2 |b_{1,2}|^2}{\rho P_2 |b_{1,2}|^2 + \sigma^2} = \frac{\rho GCP_2}{\rho GCP_2 + \sigma^2(x^2 + y^2 + (z - h_{\text{BS}})^2)(x^2 + (d - y)^2 + (z - h_{\text{BS}})^2)}, \quad (\text{C5})$$

$$D_2 \triangleq \frac{\rho P_1 |b_{2,1}|^2}{\rho P_1 |b_{2,1}|^2 + \sigma^2} = \frac{\rho GCP_1}{\rho GCP_1 + \sigma^2(x^2 + y^2 + (z - h_{\text{BS}})^2)(x^2 + (d - y)^2 + (z - h_{\text{BS}})^2)}, \quad (\text{C6})$$

$$E_1 \triangleq \frac{\partial D_1}{\partial d} = \frac{-2\rho\sigma^2 GCP_2 (d - y)(x^2 + y^2 + (z - h_{\text{BS}})^2)}{(\rho GCP_2 + \sigma^2(x^2 + y^2 + (z - h_{\text{BS}})^2)(x^2 + (d - y)^2 + (z - h_{\text{BS}})^2))^2}, \quad (\text{C7})$$

$$E_2 \triangleq \frac{\partial D_2}{\partial d} = \frac{-2\rho\sigma^2 GCP_1 (d - y)(x^2 + y^2 + (z - h_{\text{BS}})^2)}{(\rho GCP_1 + \sigma^2(x^2 + y^2 + (z - h_{\text{BS}})^2)(x^2 + (d - y)^2 + (z - h_{\text{BS}})^2))^2}, \quad (\text{C8})$$

and using the chain rule for derivation, the partial derivative of $P_{\text{D}}(x, y, z)$ with respect to inter-site distance d are first calculated as follows

$$\begin{aligned} \frac{\partial P_{\text{D}}(x, y, z)}{\partial d} &= \sqrt{\frac{L}{4\pi}} \cdot \left(\frac{\partial \text{SINR}_1(x, y, z)}{\partial d} + E_1 \right) \cdot \frac{\exp\left(\frac{-\sqrt{2L}(\text{SINR}_1(x, y, z) + D_1) - \kappa}{2}\right)}{\sqrt{\text{SINR}_1(x, y, z) + D_1}} \cdot Q\left(\sqrt{2L(\text{SINR}_2(x, y, z) + D_2)} - \kappa\right) \\ &+ \sqrt{\frac{L}{4\pi}} \cdot \left(\frac{\partial \text{SINR}_2(x, y, z)}{\partial d} + E_2 \right) \cdot \frac{\exp\left(\frac{-\sqrt{2L}(\text{SINR}_2(x, y, z) + D_2) - \kappa}{2}\right)}{\sqrt{\text{SINR}_2(x, y, z) + D_2}} \cdot Q\left(\sqrt{2L(\text{SINR}_1(x, y, z) + D_1)} - \kappa\right). \end{aligned} \quad (\text{C9})$$

Similarly, by using the derivation formula for integrals with parameters, the partial derivative of the average joint detection probability with respect to the inter-site distance d can be expressed as

$$\begin{aligned} \frac{\partial \overline{P_{\text{D}}}}{\partial d} &= \frac{1}{(\beta - \alpha)x_0(h_{\text{max}} - h_{\text{min}})} \frac{\partial \int_{\alpha d}^{\beta d} dy \int_0^{x_0} dx \int_{h_{\text{min}}}^{h_{\text{max}}} \frac{1}{d} P_{\text{D}}(x, y, z) dz}{\partial d} \\ &= \frac{1}{(\beta - \alpha)x_0(h_{\text{max}} - h_{\text{min}})} \int_{\alpha d}^{\beta d} dy \int_0^{x_0} dx \int_{h_{\text{min}}}^{h_{\text{max}}} \left(-\frac{1}{d^2} P_{\text{D}}(x, y, z) + \frac{1}{d} \frac{\partial P_{\text{D}}(x, y, z)}{\partial d}\right) dz \\ &+ \frac{\beta}{(\beta - \alpha)x_0(h_{\text{max}} - h_{\text{min}})} \int_0^{x_0} dx \int_{h_{\text{min}}}^{h_{\text{max}}} \frac{1}{d} P_{\text{D}}(x, \beta d, z) dz - \frac{\alpha}{(\beta - \alpha)x_0(h_{\text{max}} - h_{\text{min}})} \int_0^{x_0} dx \int_{h_{\text{min}}}^{h_{\text{max}}} \frac{1}{d} P_{\text{D}}(x, \alpha d, z) dz. \end{aligned} \quad (\text{C10})$$

It is worth noting that the above integrals cannot be solved analytically, so we use numerical methods to calculate the above integrals.

References

- 1 Hua M, Wu Q Q, He C, et al. Joint active and passive beamforming design for IRS-aided radar-communication. *IEEE Trans Wirel Commun*, 2022, 22: 2278-2294.
- 2 Chalise BK, Amin MG, Himed B. Performance tradeoff in a unified passive radar and communications system. *IEEE Signal Process Lett*, 2017, 24: 1275-1279.
- 3 H. V. Poor. *An Introduction to Signal Detection and Estimation*. Berlin, Germany: Springer, 2013.