

# Fault detection and isolation for linear parameter-varying systems with time-delays: a geometric approach

Zhao ZHANG &amp; Xiao HE\*

*Department of Automation, Tsinghua University, Beijing 100084, China*

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**Abstract** Fault detection and isolation (FDI) problems for linear parameter-varying (LPV) systems with state time-delays are studied in this paper. By defining the concept of unobservability subspace and designing its calculation algorithm, the geometric approach is introduced to the time-delay LPV systems. Utilizing Wirtinger-based integral inequality, we obtain a sufficient condition to solve the so-called  $H_\infty$ -based residual generation problem for the LPV systems. In this paper, we consider two cases: the time delay is known and the time delay is unknown but its estimated value can be obtained. Corresponding observers are proposed for both cases based on the geometric approach and  $H_\infty$  techniques. Lyapunov-Krasovskii functional is utilized to handle the time-delays and Wirtinger's inequality is employed to reduce conservatism. Numerical examples are presented to demonstrate the effectiveness of the proposed approach.

**Keywords** time-delay LPV systems, geometric approach, fault detection and isolation, exact-memory, rough-memory

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## 1 Introduction

System faults may pose severe challenges to the safety of the system and lead to disastrous consequences. In some safety-critical systems, such as aerospace, deep-sea manned submersible, high-speed aircraft, and chemical processes, safety and reliability are important factors for system design and operation [1–5]. Therefore, it is necessary to carry out fault diagnosis, which can provide fault information for subsequent operations (e.g., fault-tolerant controllers) to eliminate or weaken the impact of faults [6–10]. Driven by the actual industrial demand, fault diagnosis has become an important research topic in the field of automatic control. In the past decades, researchers have carried out extensive research on fault diagnosis techniques and published a series of results in this area [11–15].

The time-delay linear parameter-varying (LPV) system has the characteristics of both LPV systems and the time-delay phenomenon, and it has a wide range of applications in practice [16–20]. Many practical systems can be modeled as time-delay LPV systems. Han et al. [21] utilized the time-delay LPV system to establish a model of the supercavitating vehicle and designed a robust predictive controller. Tasoujian et al. [22] adopted the state-delay LPV system to describe the mean arterial blood pressure dynamics, and they used the Bayesian-based multiple-model square-root cubature Kalman filtering approach to estimate the varying parameters and delay. Zhang et al. [23] modeled the milling process as a time-delay LPV system and analyzed the system stability. It can be seen that the study of time-delay LPV systems is of wide practical importance. However, most existing results are about system controller design, and there is a lack of research on fault diagnosis.

In terms of fault diagnosis of time-delay LPV systems, some research results have been published. Hassanabadi et al. [24] designed a proportional-integral unknown input observer to estimate the actuator

\* Corresponding author (email: hexiao@tsinghua.edu.cn)

fault for singular delayed LPV systems. Hamdi et al. [25] proposed an adaptive polytopic observer to detect time-varying faults. Combined with set theory, a set-theoretic unknown input observer was put forward for robust fault detection for LPV systems in [26]. In most existing results, a common assumption is that only one fault occurs at the same time. The main purpose is to detect whether the fault occurs or estimate the fault amplitude. When there are multiple faults in the system, the mentioned methods cannot effectively isolate different faults. In linear time-invariant systems, an effective fault detection and isolation (FDI) method is the geometric fault observer, which was proposed by Massoumnia et al. [27,28]. Thanks to the excellent properties of the geometric fault observer, it has been generalized to solve the FDI problems for LPV systems by Bokor et al. [29,30]. However, they did not consider time-delays, and to the best of the author's knowledge, there have been no results in introducing the geometric approach to time-delay LPV systems. The analysis and design of geometric approach-based FDI observers for time-delay LPV systems is still a challenging problem.

In response to the above discussions, we consider the FDI problem for time-delay LPV systems in this paper to handle the following challenges: (1) How to introduce the geometric concepts to time-delay LPV systems for detecting and isolating multiple faults? (2) How to deal with the influence of time-delays on observer design? The basic goal of this paper is to provide a satisfactory solution to the above two questions. The main contributions of this paper are summarized as follows: (1) We propose the concepts of time-delay parameter-varying conditioned invariant subspace (TPCIS) and time-delay parameter-varying unobservability subspace (TPUS), and put forward their calculation algorithms. The geometric approach is successfully introduced to the time-delay LPV systems. (2) We consider two cases where the time-delay is known and the time-delay is unknown but its estimated value can be obtained. Fault diagnosis observers are designed for both cases based on the geometric approach and  $H_\infty$  techniques, respectively. (3) Lyapunov-Krasovskii functional is utilized to handle the time-delays and Wirtinger's inequality is employed to reduce conservatism.

The rest of the paper is outlined as follows. In Section 2, we formulate the considered problem. Section 3 introduces the concepts of TPCIS and TPUS and their geometric properties. Next, we design a set of FDI observers based on the geometric approach together with  $H_\infty$  techniques and obtain the sufficient conditions in Section 4 with the assumption that the time-delay is precisely known and the time-delay is unknown, respectively. The effectiveness of the proposed approach is illustrated through two numerical simulations in Section 5. Finally, we conclude this paper in Section 6.

**Notation.** Script letters, e.g.  $\mathcal{X}, \mathcal{Y}$ , represent real vector spaces.  $X^{-r}$  stands for the right inverse of  $X$ .  $\mathcal{L}$  is used to refer to the range of  $L$  and  $\ker C$  refers to the kernel space of  $C$ .  $P \succ 0$  represents that  $P$  is symmetric and positive definite. For any square matrix  $X \in \mathbb{R}^{n \times n}$ ,  $\text{He}(X) = X + X^T$ . The mark  $*$  is used to represent a matrix that can be complemented by symmetry.  $\|x\|_{L_2} = (\int_0^\infty x^T(t)x(t)dt)^{1/2}$  is the  $L_2$ -norm of  $x(t)$ .  $\mathcal{X}^\perp$  denotes the orthogonal complement of subspace  $\mathcal{X}$ .  $\mathbf{k}$  is defined as the set  $\{1, 2, \dots, k\}$ . A matrix  $X(\rho(t))$  is said to be an affine function with respect to  $\rho(t)$  if it can be described as  $X(\rho(t)) = X_0 + \rho_1(t)X_1 + \dots + \rho_{n_\rho}(t)X_{n_\rho}$ . The notation  $\text{diag}(A, B)$  represents a block diagonal matrix composed of  $A$  and  $B$ .

## 2 Problem formulation

Consider the following state time-delay LPV system:

$$\begin{aligned} \dot{x}(t) &= A(\rho(t))x(t) + A_\tau(\rho(t))x(t - \tau(t)) + B(\rho(t))u(t) + B^d(\rho(t))d(t) + \sum_{i=1}^k L_i(\rho(t))m_i(t), \\ y(t) &= Cx(t) + D^d d(t), \\ x(\theta) &= \phi(\theta), \quad \theta \in [-\tau_M, 0], \end{aligned} \quad (1)$$

where  $x \in \mathcal{X}$  is the state with dimension  $n_x$ ,  $y \in \mathcal{Y}$  is the output with dimension  $n_y$ ,  $u(t)$  is the input with dimension  $n_u$ , and  $d(t)$  is the disturbance with dimension  $n_d$ .  $m_i \in \mathcal{M}_i$ ,  $i \in \mathbf{k}$  is the fault mode with dimension  $n_m^i$ , and  $L_i(\rho(t))$  is the fault signature that is affine with respect to the scheduling parameters. Without loss of generality, we consider that there are  $k$  possible faults.  $\tau(t)$  denotes the time-varying delay with  $\tau(t) \in [\tau_m, \tau_M]$ , where  $\tau_m$  and  $\tau_M$  are the minimal and maximal values of possible delays. The output matrix  $C$  is right invertible,  $D^d$  is a constant matrix, and system matrices  $A(\rho(t)), A_\tau(\rho(t)),$

$B(\rho(t))$ , and  $B^d(\rho(t))$  are all affine functions.  $\rho_i(t), i = 1, \dots, n_\rho$  denotes the time-varying parameter. It is assumed that each parameter  $\rho_i(t)$  varies between known extremal values  $\rho_i(t) \in [\underline{\rho}_i, \bar{\rho}_i]$ . The parameter set, which consists of all vectors  $\rho(t) \triangleq [\rho_1(t), \dots, \rho_{n_\rho}(t)], t \in [t_0, t_1]$ , is defined as  $\mathcal{P}$ . For convenience and simplicity of expression, we use  $\rho$  to represent  $\rho(t)$ .

**Assumption 1.** It is assumed that the time-varying parameters are unknown but the current values can be obtained in real time.

**Assumption 2.** The disturbance signal  $d(t)$  is  $L_2$ -norm bounded.

**Assumption 3.** The time delay  $\tau(t)$  is time-varying and satisfies the following constraints:

$$\tau(t) \in [\tau_m, \tau_M], \dot{\tau}(t) \in [\varsigma_m, \varsigma_M], \forall t \geq 0, \tag{2}$$

where  $0 \leq \tau_m \leq \tau_M$  and  $\varsigma_m \leq \varsigma_M < 1$ .

The main objective of this paper is to detect and isolate different faults for time-delay LPV systems based on the geometric approach. To achieve this goal, we need first to propose the basic geometric concepts including TPCIS and TPUS, and introduce the geometric approach to time-delay LPV systems. Based on the geometric approach together with  $H_\infty$  techniques, a set of observers will be designed to detect and isolate different faults.

### 3 Unobservability subspace

In this section, some relevant concepts in the geometric approach, including invariant subspace and unobservability subspace of state time-delay LPV systems, are summarized.

**Definition 1.** A subspace  $\mathcal{V}$  is called a state time-delay parameter-varying invariant subspace (TPIS) for the family of linear maps  $A(\rho)$  and  $A_\tau(\rho)$  (denoted by  $[A(\rho), A_\tau(\rho)]$ -invariant subspace) if

$$A(\rho)\mathcal{V} \subseteq \mathcal{V}, A_\tau(\rho)\mathcal{V} \subseteq \mathcal{V}, \forall \rho \in \mathcal{P}. \tag{3}$$

The following lemma is useful for introducing the unobservability subspace for the state time-delay LPV systems.

**Lemma 1** ([31]). Any state trajectory  $x(t), t \in [t_0, t_1]$  belongs to a subspace  $\mathcal{L} \subseteq \mathcal{X}$  if and only if  $x(t_0) \in \mathcal{L}$  and  $\dot{x}(t) \in \mathcal{L}$  almost everywhere (a.e.) in  $[t_0, t_1]$ .

Based on Lemma 1, we have the following result.

**Lemma 2.** Consider the following LPV system with state time-delays:

$$\begin{aligned} \dot{x}(t) &= A(\rho)x(t) + A_\tau(\rho)x(t - \tau(t)), \\ x(\theta) &= \phi(\theta), \theta \in [-\tau_M, 0]. \end{aligned} \tag{4}$$

Let  $\mathcal{V} \subseteq \mathcal{X}$  be a  $[A(\rho), A_\tau(\rho)]$ -invariant subspace for all  $\rho \in \mathcal{P}$ . If  $\phi(\theta) \in \mathcal{V}, \forall \theta \in [-\tau_M, 0]$ , then  $x(t) \in \mathcal{V}$  a.e. for  $t \geq 0$ .

*Proof.* First, let us show that if  $\phi(\theta) \in \mathcal{V}, \forall \theta \in [-\tau_M, 0]$ , then  $\dot{\phi}(\theta) \in \mathcal{V}, \forall \theta \in [-\tau_M, 0]$ . It is known that a Lebesgue measurable and integrable function is zero a.e. in  $[t_0, t_1]$  if and only if its integral in any subinterval of  $[t_0, t_1]$  is zero. By applying this property to the function  $Y^T \dot{\phi}(\theta)$ , where  $Y$  is a basis of the subspace  $\mathcal{V}^\perp$ , we can get

$$\int_{-\tau_M}^\theta Y^T \dot{\phi}(\theta) dt = Y^T (\phi(\theta) - \phi(-\tau_M)) = 0.$$

This indicates that  $\dot{\phi}(\theta) \in \mathcal{V}, \theta \in [-\tau_M, 0]$  holds a.e.. In addition,  $\dot{x}(0^+) = A(\rho)x(0) + A_\tau(\rho)x(-\tau(t)) \in \mathcal{V}$ . Based on Lemma 1, we have  $x(0^+) \in \mathcal{V}$ . Similarly, it can be shown that  $x(t) \in \mathcal{V}, t \geq 0$  by successive application of this process. This concludes the proof.

**Remark 1.** Meskin et al. [32, 33] proposed similar results for linear time-delay systems. Inspired by these studies, we put forward Lemma 2 for LPV time-delay systems.

Without loss of generality, we ignore the system input and disturbance when introducing the geometric concepts. In general, the following observers are designed to detect system faults:

$$\begin{aligned} \dot{\hat{x}}(t) &= A(\rho)\hat{x}(t) + A_\tau(\rho)\hat{x}(t - \tau(t)) + D(\rho)(\hat{y}(t) - y(t)) + D_\tau(\rho)(\hat{y}(t - \tau(t)) - y(t - \tau(t))), \\ \hat{y}(t) &= C\hat{x}(t), \\ \hat{x}(\theta) &= \phi(\theta), \theta \in [-\tau_M, 0], \end{aligned} \tag{5}$$

where  $D(\rho)$  and  $D_\tau(\rho)$  are observer matrices with affine form.

In general,  $e(t) = \hat{x}(t) - x(t)$  is set to represent the estimation error. The residual can be designed as a linear mixture of the estimation error, that is,  $r(t) = H(\hat{y}(t) - y(t))$ . The dynamic equation of the residual can be obtained as follows:

$$\begin{aligned} \dot{e}(t) &= (A(\rho) + D(\rho)C)e(t) + (A_\tau(\rho) + D_\tau(\rho)C)e(t - \tau(t)) - \sum_{i=1}^k L_i(\rho)m_i(t), \\ r(t) &= HCe(t). \end{aligned}$$

As can be seen in Section 4, the unobservability subspace plays an important role in the FDI problem of time-delay LPV systems. Aiming to introduce the definition of unobservability subspace, we first introduce the notation of TPCIS for given pairs of matrices  $(C, A(\rho), A_\tau(\rho))$ .

**Definition 2.** A subspace  $\mathcal{W} \subseteq \mathcal{X}$  is called a TPCIS for the pairs of the linear maps  $C, A(\rho)$ , and  $A_\tau(\rho)$  (denoted by  $[C, A(\rho), A_\tau(\rho)]$ -invariant subspace) if any one of the following equivalent conditions holds:

(1) For  $\forall \rho \in \mathcal{P}$ ,

$$A(\rho)(\mathcal{W} \cap \ker C) \subseteq \mathcal{W}, \quad A_\tau(\rho)(\mathcal{W} \cap \ker C) \subseteq \mathcal{W}.$$

(2) There exist matrices  $D(\rho)$  and  $D_\tau(\rho)$  such that for  $\forall \rho \in \mathcal{P}$ ,

$$(A(\rho) + D(\rho)C)\mathcal{W} \subseteq \mathcal{W}, \quad (A_\tau(\rho) + D_\tau(\rho)C)\mathcal{W} \subseteq \mathcal{W}.$$

**Remark 2.** The equivalence of the two conditions in Definition 2 can be proved through a similar method as in Subsection 4.1 in [31], which is omitted here.

Let  $\mathcal{S} \subseteq \mathcal{X}$  be the largest  $[C, A(\rho), A_\tau(\rho)]$ -invariant subspace that is contained in  $\ker HC$ . According to Lemmas 1 and 2, for any initial condition  $\phi(\theta) \in \mathcal{S}, \forall \theta \in [-\tau_M, 0]$ , we have  $r(t) = 0, \forall t \geq 0$  when there is no fault. Based on this conclusion, we define the notion of parameter-varying unobservability subspace for the time-delay LPV systems as follows.

**Definition 3.** A subspace  $\mathcal{S} \subseteq \mathcal{X}$  is called a TPUS for the state time-delay LPV system (denoted by  $[C, A(\rho), A_\tau(\rho)]$ -unobservability subspace) if there exist output injection maps  $D(\rho)$  and  $D_\tau(\rho)$  and measurement mixing map  $H$  such that for  $\forall \rho \in \mathcal{P}$ ,

$$\mathcal{S} = \langle \ker HC | A(\rho) + D(\rho)C, A_\tau(\rho) + D_\tau(\rho)C \rangle, \tag{6}$$

where  $\langle \ker HC | A(\rho) + D(\rho)C, A_\tau(\rho) + D_\tau(\rho)C \rangle$  denotes the largest  $[C, A(\rho), A_\tau(\rho)]$ -invariant subspace that is contained in  $\ker HC$ . Based on this definition, we can see that unobservability subspace  $\mathcal{S}$  is related to maps  $D(\rho), D_\tau(\rho)$ , and  $H$ . For a given unobservability subspace  $\mathcal{S}$ , the map  $H$  can be calculated by the equation  $\ker HC = \ker C + \mathcal{S}$ .

**Remark 3.** According to Definitions 2 and 3, TPCIS and TPUS are subspaces that are determined by system matrices  $C, A(\rho)$ , and  $A_\tau(\rho)$ . The construction and properties of these subspaces are not affected by system disturbances.

It can be found that the unobservability subspace is a  $[A(\rho) + D(\rho)C, A_\tau(\rho) + D_\tau(\rho)C]$ -invariant subspace, and it is contained in  $\ker HC$ . Based on this property, we give a brief illustration of the geometric approach. Suppose we want to detect and isolate the  $i$ -th fault  $m_i$  among all the possible  $k$  faults. Then if there exists an unobservability subspace that contains all the other fault spaces, we can design a suitable observer such that the effects of all the other faults remain zero in the residual. Thus, we can successfully detect and isolate the  $i$ -th fault.

From the perspective of practical application, it is an important requirement to describe the characteristics of the above subspaces with a limited number of conditions. If we assume that matrices  $A(\rho)$  and  $A_\tau(\rho)$  satisfy affine structure, it is obvious that if the conditions hold for all  $A_i$  and  $A_{\tau,i}$ , then they also hold for all  $A(\rho)$  and  $A_\tau(\rho), \forall \rho \in \mathcal{P}$ .

**Lemma 3** ([29]). Assume that the functions  $\rho_i(t), i = 1, \dots, n_\rho$  are linearly independent. Then for any subspaces  $\mathcal{V}_1, \mathcal{V}_2$ , and affine function  $A(\rho), A(\rho)\mathcal{V}_1 \subseteq \mathcal{V}_2$  holds for  $\forall \rho \in \mathcal{P}$  if and only if

$$A_i \mathcal{V}_1 \subseteq \mathcal{V}_2, \quad i = 0, \dots, n_\rho. \tag{7}$$

We employ  $\underline{D}(\rho)(\mathcal{W})$  and  $\underline{D}_\tau(\rho)(\mathcal{W})$  to represent the family of all maps  $D(\rho)$  and  $D_\tau(\rho)$  satisfying  $(A(\rho) + D(\rho)C)\mathcal{W} \subseteq \mathcal{W}$  and  $(A_\tau(\rho) + D_\tau(\rho)C)\mathcal{W} \subseteq \mathcal{W}$ , respectively. Suppose  $\mathcal{L} \subseteq \mathcal{X}$  is a subspace. Let  $\underline{\mathcal{W}}(\mathcal{L})$  denote the class of  $[C, A(\rho), A_\tau(\rho)]$ -invariant subspaces containing  $\mathcal{L}$ . It should be pointed out that  $\underline{\mathcal{W}}(\mathcal{L})$  is closed under intersection, which means that  $\underline{\mathcal{W}}(\mathcal{L})$  contains a minimal subspace  $\mathcal{W}^* \triangleq \inf \underline{\mathcal{W}}(\mathcal{L})$ . In order to calculate  $\mathcal{W}^*$ , a recursive algorithm is proposed as shown below:

$$\begin{aligned} \mathcal{W}_0 &= \mathcal{L}, \\ \mathcal{W}_k &= \mathcal{L} + \sum_{i=0}^{n_\rho} A_i(\mathcal{W}_{k-1} \cap \ker C) + \sum_{i=0}^{n_\rho} A_{\tau,i}(\mathcal{W}_{k-1} \cap \ker C). \end{aligned}$$

The above algorithm converges in finite steps, and the limit value is  $\lim \mathcal{W}_k$ . We have  $\mathcal{W}^* = \lim \mathcal{W}_k$ .

The notation  $\underline{\mathcal{S}}(\mathcal{L})$  is employed to denote the set of  $[C, A(\rho), A_\tau(\rho)]$ -unobservability subspaces containing a subspace  $\mathcal{L} \subseteq \mathcal{X}$ . Similar to  $\underline{\mathcal{W}}(\mathcal{L})$ ,  $\underline{\mathcal{S}}(\mathcal{L})$  is also closed under intersection, which means that there is a minimum element  $\mathcal{S}^* \triangleq \inf \underline{\mathcal{S}}(\mathcal{L})$ . A recursive algorithm is proposed to calculate  $\mathcal{S}^*$  as shown below:

$$\begin{aligned} \mathcal{S}_0 &= \mathcal{X}, \\ \mathcal{S}_k &= \left[ \mathcal{W}^* + \left( \bigcap_{i=0}^{n_\rho} (A_i^{-1} \mathcal{S}_{k-1}) \right) \cap \ker C \right] \cap \left[ \mathcal{W}^* + \left( \bigcap_{i=0}^{n_\rho} (A_{\tau,i}^{-1} \mathcal{S}_{k-1}) \right) \cap \ker C \right]. \end{aligned}$$

The given algorithm converges in finite steps, and the limit value is  $\lim \mathcal{S}_k$ . We have  $\mathcal{S}^* = \lim \mathcal{S}_k$ .

**Remark 4.** For brevity, the construction of the subspaces is not detailed here. For more details, refer to [30, 32–34].

## 4 $H_\infty$ -based geometric FDI observer

### 4.1 Observer design with exact-memory

In this subsection, we assume that the time delay  $\tau(t)$  is precisely known. For each fault mode, we design a reduced-order observer as shown below to generate residual signals.

$$\begin{aligned} \dot{w}_i(t) &= N_i(\rho)w_i(t) + N_{i\tau}(\rho)w_i(t - \tau(t)) - G_i(\rho)y(t) - G_{i\tau}(\rho)y(t - \tau(t)) + F_i(\rho)u(t), \\ r_i(t) &= M_i w_i(t) - H_i y(t), \\ w_i(\theta) &= \phi_i(\theta), \quad \theta \in [-\tau_M, 0], \end{aligned} \tag{8}$$

where  $w_i$  is the state of the observer and  $r_i$  is the residual signal.  $N_i(\rho)$ ,  $N_{i\tau}(\rho)$ ,  $G_i(\rho)$ ,  $G_{i\tau}(\rho)$ , and  $F_i(\rho)$  are the parameter matrices with affine form.  $M_i$  and  $H_i$  are constant matrices.

Let  $e_i(t) = w_i(t) - P_{c_i}x(t)$ , where  $P_{c_i}$  is a canonical projection. Now, we present a detailed description of the problem considered in this paper. The  $H_\infty$ -based residual generation problem for the state time-delay LPV system (1) (marked as “HRGP-dLPV”) is to construct a set of observers (8) to generate residuals that satisfy the following conditions.

- (1)  $m_i \mapsto r_j = 0$ , when  $i \neq j$ ;
- (2)  $m_i \mapsto r_j$  is input observable, when  $i = j$ ;
- (3) when  $m_i = 0$ ,  $d \neq 0$ , and the initial conditions are zero, the following inequality holds:

$$\|r_i\|_{L_2} < \gamma_i \|d\|_{L_2}, \tag{9}$$

where  $\gamma_i$  is a scalar.

**Remark 5.** Conditions (1) and (2) of HRGP-dLPV mean that the output of  $i$ -th observer  $r_i$  is only sensitive to fault  $m_i$  and robust to all the other faults  $m_j, j \neq i$ .

The following lemmas are introduced to derive our main results.

**Lemma 4** ([35]). Consider an integral quadratic term of the form

$$\ell_R(\omega) = \int_a^b \omega^T(s)R\omega(s)ds,$$

where  $-\infty < a < b < +\infty$  are scalars,  $\omega$  is a continuous function from  $[a, b] \rightarrow \mathbb{R}^n$  and consequently integrable. With a given matrix  $R \succ 0$ , the following inequality holds for all continuously differentiable function  $\omega$  in  $[a, b] \rightarrow \mathbb{R}^n$ :

$$\ell_R(\dot{\omega}) \geq \frac{1}{b-a} (\omega(b) - \omega(a))^T R (\omega(b) - \omega(a)) + \frac{3}{b-a} \Omega^T R \Omega,$$

where  $\Omega = \omega(b) + \omega(a) - \frac{2}{b-a} \int_a^b \omega(s) ds$ .

**Lemma 5** ([36]). For given positive integers  $n, m$ , a scalar  $\alpha$  in the interval  $[0, 1]$ , a given  $n \times n$ -matrix  $R \succ 0$ , two matrices  $W_1$  and  $W_2$  in  $\mathbb{R}^{n \times m}$ , define, for all vector  $\xi$  in  $\mathbb{R}^m$ , the function  $\Theta(\alpha, R)$  as

$$\Theta(\alpha, R) = \frac{1}{\alpha} \xi^T W_1^T R W_1 \xi + \frac{1}{1-\alpha} \xi^T W_2^T R W_2 \xi.$$

If there exists a matrix  $X$  in  $\mathbb{R}^{n \times n}$  such that  $\begin{bmatrix} R & X \\ * & R \end{bmatrix} \succ 0$ , then the following inequality holds:

$$\min_{\alpha \in (0,1)} \Theta(\alpha, R) \geq \begin{bmatrix} W_1 \xi \\ W_2 \xi \end{bmatrix}^T \begin{bmatrix} R & X \\ * & R \end{bmatrix} \begin{bmatrix} W_1 \xi \\ W_2 \xi \end{bmatrix}.$$

**Remark 6.** Lemma 4 is an inequality derived from Wirtinger’s inequality, which is less conservative compared with Jensen’s inequality [35].

According to the analysis of TPUS in Section 3, the geometric approach is introduced into time-delay LPV systems to separate different fault spaces. Based on this property, we can achieve fault detection and isolation simultaneously. Regarding system disturbances, we employ  $H_\infty$  techniques to suppress their effects. Considering the state time-delay LPV system (1) with  $u(t) \equiv 0$  and  $m_i(t) \equiv 0, \forall t \geq 0$ , we have the following result.

**Theorem 1.** Assume that there exist  $n \times n$ -matrices  $P \succ 0, S \succ 0, Q \succ 0, R \succ 0$ , a  $2n \times 2n$ -matrix  $X$ , and a scalar  $\gamma > 0$  such that the following matrix inequalities are satisfied for  $\tau = \{\tau_m, \tau_M\}$  and  $\dot{\tau} = \{\varsigma_m, \varsigma_M\}$ :

$$\Phi_0(\tau, \dot{\tau}) = \Phi_1(\tau, \dot{\tau}) - \frac{1}{\tau_M} \Gamma^T \Phi_2 \Gamma - \Phi_3 \prec 0, \quad \Phi_2 = \begin{bmatrix} \tilde{R} & X \\ * & \tilde{R} \end{bmatrix} \succ 0, \tag{10}$$

where

$$\begin{aligned} \Phi_1(\tau, \dot{\tau}) &= \text{He} \left( G_1^T(\tau) \hat{P} G_0(\dot{\tau}) \right) + \hat{S} + \hat{Q}(\dot{\tau}) + \tau_M G_0^T(\dot{\tau}) \hat{R} G_0(\dot{\tau}), \quad \Gamma = \begin{bmatrix} G_2^T & G_3^T & G_4^T & G_5^T \end{bmatrix}^T, \\ \Phi_3 &= \begin{bmatrix} -C^T C & 0 & 0 & 0 & 0 & -C^T D^d \\ * & 0 & 0 & 0 & 0 & 0 \\ * & * & 0 & 0 & 0 & 0 \\ * & * & * & 0 & 0 & 0 \\ * & * & * & * & 0 & 0 \\ * & * & * & * & * & \gamma^2 I - (D^d)^T D^d \end{bmatrix}, \\ G_2 &= \begin{bmatrix} I & -I & 0 & 0 & 0 & 0 \end{bmatrix}, \quad G_3 = \begin{bmatrix} I & I & 0 & -2I & 0 & 0 \end{bmatrix}, \quad G_4 = \begin{bmatrix} 0 & I & -I & 0 & 0 & 0 \end{bmatrix}, \quad G_5 = \begin{bmatrix} 0 & I & I & 0 & -2I & 0 \end{bmatrix}, \\ \hat{P} &= \text{diag}(P, P, P), \quad \hat{Q}(\dot{\tau}) = \text{diag}(Q, -(1-\dot{\tau})Q, 0_{4n}), \\ \hat{S} &= \text{diag}(S, 0, -S, 0_{3n}), \quad \hat{R} = \text{diag}(R, 0_{2n}), \quad \tilde{R} = \text{diag}(R, 3R), \\ G_0(\dot{\tau}) &= \begin{bmatrix} A(\rho) & A_\tau(\rho) & 0 & 0 & 0 & B^d(\rho) \\ I & -(1-\dot{\tau})I & 0 & 0 & 0 & 0 \\ 0 & (1-\dot{\tau})I & -I & 0 & 0 & 0 \end{bmatrix}, \quad G_1(\tau) = \begin{bmatrix} I & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & \tau I & 0 & 0 \\ 0 & 0 & 0 & 0 & (\tau_M - \tau) I & 0 \end{bmatrix}. \end{aligned}$$

Then the system (1) with  $u(t) \equiv 0$  and  $m_i(t) \equiv 0$  satisfies  $\|y\|_{L_2} < \gamma \|d\|_{L_2}$ .

*Proof.* Consider the Lyapunov-Krasovskii functional as follows:

$$V = \tilde{x}^T(t)\hat{P}\tilde{x}(t) + \int_{t-\tau(t)}^t x^T(\eta)Qx(\eta)d\eta + \int_{t-\tau_M}^t x^T(\eta)Sx(\eta)d\eta + \int_{t-\tau_M}^t \int_{\theta}^t \dot{x}^T(\eta)R\dot{x}(\eta)d\eta d\theta,$$

where  $\tilde{x}(t) \triangleq [x^T(t), \int_{t-\tau(t)}^t x^T(\eta)d\eta, \int_{t-\tau_M}^{t-\tau(t)} x^T(\eta)d\eta]^T$ .

The derivative of the function along the trajectory of (1) leads to

$$\begin{aligned} \dot{V} = & \dot{\tilde{x}}^T(t)\hat{P}\tilde{x}(t) + \tilde{x}^T(t)\hat{P}\dot{\tilde{x}}(t) + x^T(t)Qx(t) - (1 - \dot{\tau}(t))x^T(t - \tau(t))Qx(t - \tau(t)) \\ & + x^T(t)Sx(t) - x^T(t - \tau_M)Sx(t - \tau_M) + \tau_M\dot{x}^T(t)R\dot{x}(t) - \int_{t-\tau_M}^t \dot{x}^T(\eta)R\dot{x}(\eta)d\eta. \end{aligned} \tag{11}$$

Let

$$\zeta_1^T(t) = \left[ x^T(t), x^T(t - \tau(t)), x^T(t - \tau_M), \frac{1}{\tau(t)} \int_{t-\tau(t)}^t x^T(\eta)d\eta, \frac{1}{\tau_M - \tau(t)} \int_{t-\tau_M}^{t-\tau(t)} x^T(\eta)d\eta, d^T(t) \right].$$

We have  $\tilde{x}(t) = G_1(\tau)\zeta_1(t)$  and  $\dot{\tilde{x}}(t) = G_0(\dot{\tau})\zeta_1(t)$ .

Next, we divide the integral term into two intervals  $[t - \tau_M, t - \tau(t)]$  and  $[t - \tau(t), t]$ , and integrate them respectively. Using Lemma 4, we can get

$$\int_{t-\tau_M}^t \dot{x}^T(s)R\dot{x}(s)ds \geq \zeta_1^T(t) \left( \frac{1}{\tau(t)} G_{2,3}^T \tilde{R} G_{2,3} + \frac{1}{\tau_M - \tau(t)} G_{4,5}^T \tilde{R} G_{4,5} \right) \zeta_1(t),$$

where  $G_{2,3} = [G_2^T \ G_3^T]^T$  and  $G_{4,5} = [G_4^T \ G_5^T]^T$ . Based on Lemma 5, if there exists a matrix  $X$  such that  $\Phi_2 = \begin{bmatrix} \tilde{R} & X \\ * & \tilde{R} \end{bmatrix} \succ 0$ , we can draw that

$$\int_{t-\tau_M}^t \dot{x}^T(s)R\dot{x}(s)ds \geq \frac{1}{\tau_M} \zeta_1^T(t) \Gamma^T \Phi_2 \Gamma \zeta_1(t).$$

With the system output equation  $y(t) = Cx(t) + D^d d(t)$ , we can deduce that

$$\gamma^2 d^T(t)d(t) - y^T(t)y(t) = \zeta_1^T(t) \Phi_3 \zeta_1(t). \tag{12}$$

According to (11) and (12), it shows

$$\dot{V} - \gamma^2 d^T(t)d(t) + y^T(t)y(t) \leq \zeta_1^T(t) \Phi_0 \zeta_1(t).$$

Therefore,

$$\dot{V} - \gamma^2 d^T(t)d(t) + y^T(t)y(t) \prec 0 \tag{13}$$

holds if there exists a matrix  $X$  such that  $\Phi_2 \succ 0$  and if  $\Phi_0 \prec 0$ , for all  $(\tau, \dot{\tau}) \in [\tau_m, \tau_M] \times [\varsigma_m, \varsigma_M]$ . Since the matrix  $\Phi_0$  is affine, and consequently convex, with respect to  $\tau(t)$  and  $\dot{\tau}(t)$ , it is necessary and sufficient to ensure that  $\Phi_0 \prec 0$  at the vertices of the intervals  $[\tau_m, \tau_M] \times [\varsigma_m, \varsigma_M]$ .

Under zero initial conditions, integrating both sides of (13) yields  $\|y\|_{L_2} < \gamma \|d\|_{L_2}$ . Consequently, the  $H_\infty$  performance is guaranteed. This concludes the proof.

Based on Theorem 1, the main result in this subsection is proposed.

**Theorem 2.** Under the assumption that the time delay  $\tau(t)$  is precisely known, the HRGP-dLPV problem has a solution if there exist  $[C, A(\rho), A_\tau(\rho)]$ -unobservability subspaces  $\mathcal{S}_i^*$  such that

$$\mathcal{L}_i \cap \mathcal{S}_i^* = 0, \quad i \in \mathbf{k}, \quad \forall \rho \in \mathcal{P}, \tag{14}$$

where  $\mathcal{S}_i^* = \inf \underline{\mathcal{S}}(\sum_{j=1, j \neq i}^k \mathcal{L}_j)$ , and there exist  $n \times n$ -matrices  $P_i \succ 0, S_i \succ 0, Q_i \succ 0, R_i \succ 0, X_{i_{11}}, X_{i_{12}}, X_{i_{21}}, X_{i_{22}}$ , continuously differentiable matrix functions  $T_{i_{p1}}(\rho), T_{i_{p2}}(\rho), T_{i_{r1}}(\rho), T_{i_{r2}}(\rho)$ , and scalars

$\gamma_i > 0$  such that the following matrix inequalities are satisfied for  $\tau = \{\tau_m, \tau_M\}$  and  $\dot{\tau} = \{\varsigma_m, \varsigma_M\}$ :

$$\Psi_{i_0}(\tau, \dot{\tau}) = \begin{bmatrix} \psi_{i_{11}} & \psi_{i_{12}} & \psi_{i_{13}} & \psi_{i_{14}} & \psi_{i_{15}} & \psi_{i_{16}} & \psi_{i_{17}} \\ * & \psi_{i_{22}} & \psi_{i_{23}} & \psi_{i_{24}} & \psi_{i_{25}} & 0 & \psi_{i_{27}} \\ * & * & \psi_{i_{33}} & \psi_{i_{34}} & \psi_{i_{35}} & 0 & 0 \\ * & * & * & \psi_{i_{44}} & \psi_{i_{45}} & 0 & 0 \\ * & * & * & * & \psi_{i_{55}} & 0 & 0 \\ * & * & * & * & * & \psi_{i_{66}} & \psi_{i_{67}} \\ * & * & * & * & * & * & \psi_{i_{77}} \end{bmatrix} \prec 0, \quad \Psi_{i_1} = \begin{bmatrix} \tilde{R}_i & X_i \\ * & \tilde{R}_i \end{bmatrix} \succ 0, \quad (15)$$

where

$$\begin{aligned} \psi_{i_{11}} &= \text{He}\{P_i A_{i_0}(\rho) + T_{i_{p1}}(\rho)M_i\} + S_i + Q_i - \frac{4}{\tau_M}R_i + M_i^T M_i, \\ \psi_{i_{12}} &= P_i A_{i_{\tau,0}}(\rho) + T_{i_{p2}}(\rho)M_i - \frac{1}{\tau_M}(2R + X_{i_{11}} + X_{i_{12}} + X_{i_{21}} + X_{i_{22}}), \\ \psi_{i_{13}} &= -\frac{1}{\tau_M}(-X_{i_{11}} - X_{i_{21}} + X_{i_{12}} + X_{i_{22}}), \quad \psi_{i_{14}} = \tau P_i + \frac{6}{\tau_M}R_i, \quad \psi_{i_{15}} = \frac{2}{\tau_M}(X_{i_{12}} + X_{i_{22}}), \\ \psi_{i_{16}} &= [\epsilon_{i_1} \quad \epsilon_{i_2}], \quad \epsilon_{i_1} = -P_i P_{c_i} D_{i_0}(\rho)D^d - T_{i_{p1}}(\rho)H_i D^d - P_i P_{c_i} B^d(\rho) + M_i^T H_i D^d, \\ \epsilon_{i_2} &= -P_i P_{c_i} D_{i_{\tau,0}}(\rho)D^d - T_{i_{p2}}(\rho)H_i D^d, \quad \psi_{i_{17}} = A_{i_0}^T(\rho)R_i + M_i^T T_{i_{r1}}(\rho), \\ \psi_{i_{22}} &= -(1 - \dot{\tau})Q_i - \frac{1}{\tau_M}(8R_i - X_{i_{11}} - X_{i_{12}}^T - X_{i_{12}} - X_{i_{21}}^T + X_{i_{21}} + X_{i_{21}}^T + X_{i_{22}} + X_{i_{22}}^T), \\ \psi_{i_{23}} &= -\frac{1}{\tau_M}(2R_i + X_{i_{11}} - X_{i_{21}} - X_{i_{12}} + X_{i_{22}}), \quad \psi_{i_{24}} = -\tau(1 - \dot{\tau})P_i + \frac{2}{\tau_M}(3R_i + X_{i_{21}}^T + X_{i_{22}}^T), \\ \psi_{i_{25}} &= (1 - \dot{\tau})(\tau_M - \tau)P_i + \frac{2}{\tau_M}(3R_i - X_{i_{12}} + X_{i_{22}}), \quad \psi_{i_{27}} = A_{i_{\tau,0}}^T(\rho)R_i + M_i^T T_{i_{r2}}(\rho), \\ \psi_{i_{33}} &= -S_i - \frac{4}{\tau_M}R_i, \quad \psi_{i_{34}} = \frac{2}{\tau_M}(-X_{i_{21}}^T + X_{i_{22}}^T), \quad \psi_{i_{35}} = -(\tau_M - \tau)P_i + \frac{6}{\tau_M}R_i, \\ \psi_{i_{44}} &= \psi_{i_{55}} = -\frac{12}{\tau_M}R_i, \quad \psi_{i_{45}} = -\frac{4}{\tau_M}X_{i_{22}}, \quad \psi_{i_{77}} = -\frac{1}{\tau_M}R_i, \\ \psi_{i_{66}} &= -\gamma_i^2 I + \begin{bmatrix} (D^d)^T H_i^T H_i D^d & 0 \\ 0 & 0 \end{bmatrix}, \quad \psi_{i_{67}} = \begin{bmatrix} \epsilon_{i_3} \\ \epsilon_{i_4} \end{bmatrix}, \quad X_i = \begin{bmatrix} X_{i_{11}} & X_{i_{12}} \\ X_{i_{21}} & X_{i_{22}} \end{bmatrix}, \quad \tilde{R}_i = \text{diag}(R_i, 3R_i), \\ \epsilon_{i_3} &= -(D^d)^T D_{i_0}^T(\rho)P_{c_i}^T R_i - (D^d)^T H_i^T T_{i_{r1}}(\rho) - (B^d(\rho))^T P_{c_i}^T R_i, \\ \epsilon_{i_4} &= -(D^d)^T D_{i_{\tau,0}}^T(\rho)P_{c_i}^T R_i - (D^d)^T H_i^T T_{i_{r2}}(\rho), \end{aligned}$$

$P_{c_i}$  is the canonical projection of  $\mathcal{X}$  on  $\mathcal{X}/\mathcal{S}_i^*$ ,  $D_{i_0}(\rho)$  is a map satisfying  $(A(\rho) + D_{i_0}(\rho)C)\mathcal{S}_i^* \subseteq \mathcal{S}_i^*$ ,  $A_{i_0}(\rho)$  is a map induced by  $A(\rho) + D_{i_0}(\rho)C$  on  $\mathcal{X}/\mathcal{S}_i^*$ ,  $D_{i_{\tau,0}}(\rho)$  is a map satisfying  $(A_\tau(\rho) + D_{i_{\tau,0}}(\rho)C)\mathcal{S}_i^* \subseteq \mathcal{S}_i^*$ ,  $A_{i_{\tau,0}}(\rho)$  is a map induced by  $A_\tau(\rho) + D_{i_{\tau,0}}(\rho)C$  on  $\mathcal{X}/\mathcal{S}_i^*$ ,  $H_i$  is calculated by  $\ker H_i C = \mathcal{S}_i^* + \ker C$ , and  $M_i$  is given by  $M_i P_{c_i} = H_i C$ .

*Proof.* If the unobservability subspaces satisfy (14), then according to the geometric approach, a set of observers satisfying conditions (1) and (2) exists. Through solving matrix inequalities (15), we get  $T_{i_{p1}}(\rho)$  and  $T_{i_{p2}}(\rho)$ . Let  $D_{i_1}(\rho) = P_i^{-1}T_{i_{p1}}(\rho)$ ,  $D_{i_{\tau,1}}(\rho) = P_i^{-1}T_{i_{p2}}(\rho)$ , and define  $N_i(\rho) = A_{i_0}(\rho) + D_{i_1}(\rho)M_i$ ,  $N_{i\tau}(\rho) = A_{i_{\tau,0}}(\rho) + D_{i_{\tau,1}}(\rho)M_i$ ,  $G_i(\rho) = P_{c_i}(D_{i_0}(\rho) + P_{c_i}^{-r}D_{i_1}(\rho)H_i)$ ,  $G_{i\tau}(\rho) = P_{c_i}(D_{i_{\tau,0}}(\rho) + P_{c_i}^{-r}D_{i_{\tau,1}}(\rho)H_i)$ , and  $F_i(\rho) = P_{c_i}B(\rho)$ . Therefore, we get the parameters of the observers. According to  $e_i = w_i - P_{c_i}x$ , we get

$$\begin{aligned} \dot{e}_i(t) &= N_i(\rho)w_i(t) + N_{i\tau}(\rho)w_i(t - \tau(t)) - P_{c_i}(D_{i_0}(\rho) + P_{c_i}^{-r}D_{i_1}(\rho)H_i)(Cx(t) + D^d d(t)) \\ &\quad - P_{c_i}(D_{i_{\tau,0}}(\rho) + P_{c_i}^{-r}D_{i_{\tau,1}}(\rho)H_i)(Cx(t - \tau(t)) + D^d d(t - \tau(t))) - P_{c_i}A(\rho)x(t) \\ &\quad - P_{c_i}A_\tau(\rho)x(t - \tau(t)) - P_{c_i}L_i(\rho)m_i(t) - P_{c_i}B^d(\rho)d(t) \\ &= N_i(\rho)w_i(t) + N_{i\tau}(\rho)w_i(t - \tau(t)) - P_{c_i}(A(\rho) + D_{i_0}(\rho)C)x(t) - P_{c_i}(A_\tau(\rho) \\ &\quad + D_{i_{\tau,0}}(\rho)C)x(t - \tau(t)) - D_{i_1}(\rho)M_i P_{c_i}x(t) - D_{i_{\tau,1}}(\rho)M_i P_{c_i}x(t - \tau(t)) \end{aligned}$$



$$\begin{aligned}
 & -\epsilon_{i_5}d(t) - \epsilon_{i_6}d(t - \tau(t)) - P_{c_i}L_i(\rho)m_i(t) \\
 & = (A_{i_0}(\rho) + D_{i_1}(\rho)M_i)e(t) + (A_{i_{\tau,0}}(\rho) + D_{i_{\tau,1}}(\rho)M_i)e(t - \tau(t)) - P_{c_i}L_i(\rho)m_i(t) \\
 & \quad - \begin{bmatrix} \epsilon_{i_5} & \epsilon_{i_6} \end{bmatrix} \begin{bmatrix} d(t) \\ d(t - \tau(t)) \end{bmatrix}, \\
 r_i(t) & = M_iw_i(t) - H_iCx(t) - H_iD^d d(t) = M_i e(t) - H_i \begin{bmatrix} D^d & 0 \end{bmatrix} \begin{bmatrix} d(t) \\ d(t - \tau(t)) \end{bmatrix},
 \end{aligned}$$

where  $\epsilon_{i_5} = P_{c_i}D_{i_0}(\rho)D^d + D_{i_1}(\rho)H_iD^d + P_{c_i}B^d(\rho)$ ,  $\epsilon_{i_6} = P_{c_i}D_{i_{\tau,0}}(\rho)D^d + D_{i_{\tau,1}}(\rho)H_iD^d$ . Based on Theorem 1, we can get a set of matrix inequalities, which contains the quadratic product term of some unknown matrices. Using Schur complements to perform an equivalent transformation, we can draw matrix inequalities (15), which concludes the proof.

### 4.2 Observer design with rough-memory

Different from Subsection 4.1, we assume that the time delay  $\tau(t)$  is not known precisely, and we can only get an estimated value  $\tilde{\tau}(t)$  in this part. Without loss of generality, we set  $\tilde{\tau}(t)$  to meet constraints (2), that is,  $\tilde{\tau}(t) \in [\tau_m, \tau_M]$ ,  $\dot{\tilde{\tau}}(t) \in [\varsigma_m, \varsigma_M]$ ,  $\forall t \geq 0$ . We assume that  $|\tilde{\tau}(t) - \tau(t)| \leq \varrho$  for some  $\varrho > 0$ , and the error signal  $\hat{x}(t) \triangleq x(t - \tilde{\tau}(t)) - x(t - \tau(t))$  is  $L_2$ -norm bounded.

For each fault mode, we design the reduced-order observer as shown below to generate residuals:

$$\begin{aligned}
 \dot{w}_i(t) & = N_i(\rho)w_i(t) + N_{i\tau}(\rho)w_i(t - \tilde{\tau}(t)) - G_i(\rho)y(t) - G_{i\tau}(\rho)y(t - \tilde{\tau}(t)) + F_i(\rho)u(t), \\
 r_i(t) & = M_iw_i(t) - H_iy(t), \\
 w_i(\theta) & = \phi_i(\theta), \theta \in [-\tau_M, 0].
 \end{aligned} \tag{16}$$

Similarly, we can draw the following conclusion.

**Theorem 3.** Under the assumption that the time delay  $\tau(t)$  is not known precisely, and only an estimated value can be obtained, the HRGP-dLPV problem has a solution if there exist  $[C, A(\rho), A_\tau(\rho)]$ -unobservability subspaces  $\mathcal{S}_i^*$  such that

$$\mathcal{L}_i(\rho) \cap \mathcal{S}_i^* = 0, \quad i \in \mathbf{k}, \quad \forall \rho \in \mathcal{P}, \tag{17}$$

where  $\mathcal{S}_i^* = \inf \underline{\mathcal{S}}(\sum_{j=1, j \neq i}^k \mathcal{L}_j)$ , and there exist  $n \times n$ -matrices  $P_i \succ 0, S_i \succ 0, Q_i \succ 0, R_i \succ 0, X_{i_{11}}, X_{i_{12}}, X_{i_{21}}, X_{i_{22}}$ , continuously differentiable matrix functions  $T_{i_{p1}}(\rho), T_{i_{p2}}(\rho), T_{i_{r1}}(\rho), T_{i_{r2}}(\rho)$ , and scalars  $\gamma_i > 0$  such that the following matrix inequalities are satisfied for  $\tilde{\tau} = \{\tau_m, \tau_M\}$  and  $\dot{\tilde{\tau}} = \{\varsigma_m, \varsigma_M\}$ :

$$\Psi_{i_0}(\tilde{\tau}, \dot{\tilde{\tau}}) = \begin{bmatrix} \psi_{i_{11}} & \psi_{i_{12}} & \psi_{i_{13}} & \psi_{i_{14}} & \psi_{i_{15}} & \psi_{i_{16}} & \psi_{i_{17}} \\ * & \psi_{i_{22}} & \psi_{i_{23}} & \psi_{i_{24}} & \psi_{i_{25}} & 0 & \psi_{i_{27}} \\ * & * & \psi_{i_{33}} & \psi_{i_{34}} & \psi_{i_{35}} & 0 & 0 \\ * & * & * & \psi_{i_{44}} & \psi_{i_{45}} & 0 & 0 \\ * & * & * & * & \psi_{i_{55}} & 0 & 0 \\ * & * & * & * & * & \psi_{i_{66}} & \psi_{i_{67}} \\ * & * & * & * & * & * & \psi_{i_{77}} \end{bmatrix} \prec 0, \quad \Psi_{i_1} = \begin{bmatrix} \tilde{R}_i & X_i \\ * & \tilde{R}_i \end{bmatrix} \succ 0, \tag{18}$$

where

$$\begin{aligned}
 \psi_{i_{16}} & = [\epsilon_{i_1} \quad \epsilon_{i_2} \quad \epsilon_{i_3}], \quad \epsilon_{i_1} = -P_iP_{c_i}D_{i_0}(\rho)D^d - T_{i_{p1}}(\rho)H_iD^d - P_iP_{c_i}B^d(\rho) + M_i^T H_i D^d, \\
 \epsilon_{i_2} & = -P_iP_{c_i}D_{i_{\tau,0}}(\rho)D^d - T_{i_{p2}}(\rho)H_iD^d, \quad \epsilon_{i_3} = P_iP_{c_i}A_\tau(\rho), \\
 \psi_{i_{66}} & = -\gamma_i^2 I + \begin{bmatrix} (D^d)^T H_i^T H_i D^d & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}, \quad \psi_{i_{67}} = \begin{bmatrix} \epsilon_{i_4} \\ \epsilon_{i_5} \\ \epsilon_{i_6} \end{bmatrix}, \\
 \epsilon_{i_4} & = -(D^d)^T D_{i_0}^T(\rho)P_{c_i}^T R_i - (D^d)^T H_i^T T_{i_{r1}}(\rho) - (B^d(\rho))^T P_{c_i}^T R_i,
 \end{aligned}$$

$$\epsilon_{i_5} = -(D^d)^T D_{i_{\tau,0}}^T(\rho) P_{c_i}^T R_i - (D^d)^T H_i^T T_{i_{\tau,2}}(\rho), \quad \epsilon_{i_6} = A_{\tau}^T(\rho) P_{c_i}^T R_i,$$

and other sub-matrices are the same as defined in Theorem 2 by replacing  $\tau(t)$  with  $\tilde{\tau}(t)$ .

*Proof.* Similar to the proof of Theorem 2, by solving matrix inequality (18), we can obtain the observer parameters  $N_i(\rho)$ ,  $N_{i\tau}(\rho)$ ,  $G_i(\rho)$ ,  $G_{i\tau}(\rho)$  and  $F_i(\rho)$ . Therefore, we get

$$\begin{aligned} \dot{e}_i(t) &= (A_{i_0}(\rho) + D_{i_1}(\rho)M_i)e(t) + (A_{i_{\tau,0}}(\rho) + D_{i_{\tau,1}}(\rho)M_i)e(t - \tilde{\tau}(t)) - P_{c_i}L_i(\rho)m_i(t) - [\epsilon_{i_7} \ \epsilon_{i_8} \ \epsilon_{i_9}] \hat{d}(t), \\ r_i(t) &= M_i e(t) - H_i \begin{bmatrix} D^d & 0 & 0 \end{bmatrix} \hat{d}(t), \end{aligned}$$

where  $\epsilon_{i_7} = P_{c_i}D_{i_0}(\rho)D^d + D_{i_1}(\rho)H_iD^d + P_{c_i}B^d(\rho)$ ,  $\epsilon_{i_8} = P_{c_i}D_{i_{\tau,0}}(\rho)D^d + D_{i_{\tau,1}}(\rho)H_iD^d$ ,  $\epsilon_{i_9} = -P_{c_i}A_{\tau}(\rho)$ , and  $\hat{d}(t) = [d(t) \ d(t - \tilde{\tau}(t)) \ \hat{x}(t)]^T$ . Similarly, based on Theorem 1 and Schur complements, we can draw matrix inequalities (18), which concludes the proof.

**Remark 7.** A series of results have been proposed to estimate the time delay of the system, for example, expectation-maximization algorithm [37], maximum likelihood optimization approach [38], adaptive identification technique [39], neural networks [40], and Bayesian-based approach [22]. An appropriate algorithm can be selected through experiments to get an estimation of the time delay, which is not discussed in detail in this article.

**Remark 8.** The matrix inequalities in Theorems 1–3 are all parameter-dependent matrix inequalities, and all the parameter-dependent matrices are affine functions of the time-varying parameters. In this work, the gridding techniques in [23] are utilized to solve these matrix inequalities.

### 4.3 Residual evaluation

According to HRGP-dLPV conditions (1) and (2),  $r_i$  is only affected by fault  $m_i$  and has successfully been decoupled from all the other faults  $m_j$ ,  $j \neq i$ . Accordingly, fault detection and fault isolation can be completed at the same time. In this subsection, the design of the evaluation function for residual signals is detailed. We choose the following residual evaluation function:

$$J_i(t) = \frac{1}{T_r} \left( \int_{t-T_r}^t r_i^T(\eta)r_i(\eta)d\eta \right)^{\frac{1}{2}}, \tag{19}$$

where  $T_r$  is the length of the evaluation time window. Subsequently, the threshold is selected as follows:

$$J_i^{\text{th}} = \sup_{m_i=0} J_i(t). \tag{20}$$

Based on the above evaluation functions and thresholds, the occurrence of a fault can be alarmed through the following decision rules:

$$\begin{aligned} J_i(t) > J_i^{\text{th}} &\Rightarrow \text{fault } m_i \text{ occurs, } i \in \mathbf{k}, \\ J_i(t) \leq J_i^{\text{th}} &\Rightarrow \text{fault } m_i \text{ dose not occur, } i \in \mathbf{k}. \end{aligned} \tag{21}$$

**Remark 9.** It should be pointed out that Eq. (20) is a theoretical guidance for selecting the threshold. When taking into account an actual experiment, Eq. (20) is not appropriate to determine the threshold. This is because the assumption that  $d(t)$  is  $L_2$ -norm bounded is a very constrained condition, and it is challenging to determine the precise value of the threshold. In practice, the threshold can be established using experiments or Monte Carlo simulations, and manually adjusted to compromise the missing alarm and the false alarm.

## 5 Numerical simulation

### 5.1 Case study I

In this subsection, we apply the proposed scheme to a widely used numerical model quoted from [41] to demonstrate the effectiveness of the strategy. The system model is shown as follows:

$$\begin{aligned} \dot{x}(t) &= \begin{bmatrix} 0 & 1+0.2\rho \\ -2 & -3+0.1\rho \end{bmatrix} x(t) + \begin{bmatrix} 0.2\rho & 0.1 \\ -0.2+0.1\rho & -0.3 \end{bmatrix} x(t-\tau(t)) + \begin{bmatrix} 0.2\rho \\ 0.1+0.1\rho \end{bmatrix} u(t) \\ &+ \begin{bmatrix} 0.2 \\ 0.2 \end{bmatrix} d(t) + \begin{bmatrix} 0 \\ 0.1 \end{bmatrix} m_1(t) + \begin{bmatrix} 0.2 \\ 0 \end{bmatrix} m_2(t), \\ y(t) &= \begin{bmatrix} 0 & 10 \\ 10 & 0 \end{bmatrix} x(t) + \begin{bmatrix} 0.1 \\ 0.1 \end{bmatrix} d(t), \end{aligned}$$

where  $\rho = \sin(t)$ ,  $\tau_m = 0$ ,  $\tau_M = 0.5$ ,  $\varsigma_m = -0.5$ , and  $\varsigma_M = 0.5$ . The system disturbance is set to  $d(t) = 2\sin(10t)\delta(t)$  during the simulation period, where  $\delta(t) \in [-0.5, 0.5]$  is a uniformly distributed random variable. The initial states are set as  $x(t) = [1, 1]^T, \forall t \in [-0.5, 0]$ . The state feedback controller in [42] is utilized to control the system. In this simulation, we consider that there are two faults, and the fault signals are set to

$$m_1(t) = \begin{cases} 2, & 20\text{ s} < t \leq 40\text{ s}, \\ 0, & \text{otherwise,} \end{cases} \quad m_2(t) = \begin{cases} 1, & 25\text{ s} < t \leq 45\text{ s}, \\ 0, & \text{otherwise.} \end{cases}$$

It can be seen that two faults exist simultaneously between 25–40 s.

#### 5.1.1 Exact-memory FDI observer

We consider that the time-delay is exactly known and apply Theorem 2 to calculate the observer matrices. Verifying the matrix inequalities (15) over a grid of 65 points yields the matrices as follows:

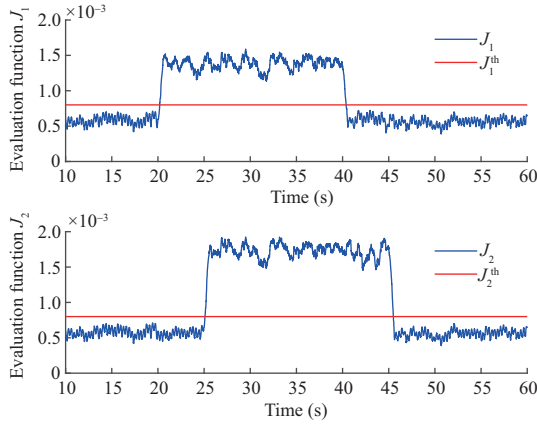
$$\begin{aligned} N_1(\rho) &= -21.9821 + 0.1\rho, \quad N_{1\tau}(\rho) = -0.3493 + 0.0653\rho, \quad F_1(\rho) = -0.1 - 0.1\rho, \quad M_1 = -1, \quad H_1 = \begin{bmatrix} 0.1 & 0 \end{bmatrix}, \\ G_1(\rho) &= \begin{bmatrix} 1.8982 & -0.2 \end{bmatrix} + \begin{bmatrix} 7.1304 \times 10^{-7} & 0 \end{bmatrix} \rho, \quad G_{1\tau}(\rho) = \begin{bmatrix} 0.0049 & -0.02 \end{bmatrix} + \begin{bmatrix} -0.0065 & 0.01 \end{bmatrix} \rho, \\ N_2(\rho) &= -17.2017 + 0.2\rho, \quad N_{2\tau}(\rho) = 0.0446 + 0.1456\rho, \quad F_2(\rho) = 0.2\rho, \quad M_2 = 1, \quad H_2 = \begin{bmatrix} 0 & 0.1 \end{bmatrix}, \\ G_2(\rho) &= \begin{bmatrix} -0.1 & -1.7202 \end{bmatrix} + \begin{bmatrix} -0.02 & 0.02 \end{bmatrix} \rho, \quad G_{2\tau}(\rho) = \begin{bmatrix} -0.01 & 0.0045 \end{bmatrix} + \begin{bmatrix} 0 & -0.0054 \end{bmatrix} \rho. \end{aligned}$$

We set the length of the evaluation window as  $T_r = 0.5$  s, and the thresholds are selected as  $J_1^{\text{th}} = J_2^{\text{th}} = 0.8 \times 10^{-3}$ . The evaluation function when two faults occur simultaneously is presented in Figure 1. As can be seen in the figure, the evaluation function  $J_1(t)$  ( $J_2(t)$ ) is only affected by the single fault  $m_1(t)$  ( $m_2(t)$ ) and not by the other fault  $m_2(t)$  ( $m_1(t)$ ), which illustrates that the proposed method can effectively detect and isolate faults in state time-delay LPV systems.

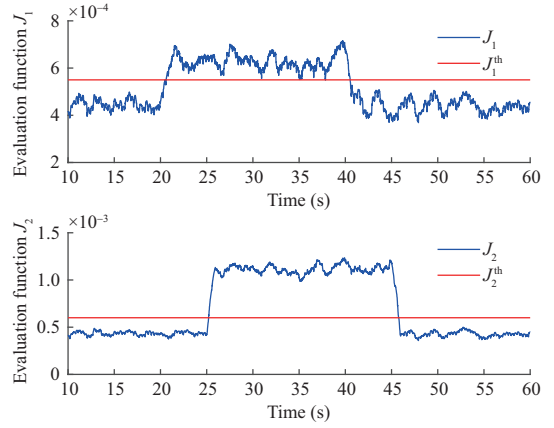
#### 5.1.2 Rough-memory FDI observer

In this part, we consider that the time-delay is unknown, and we can get an estimated value. We set  $\rho = \frac{\tau_M - \tau_m}{2}$ . Same as the previous part, verifying the matrix inequalities (18) of Theorem 3 over a grid of 65 points yields the observer parameter matrices as follows:

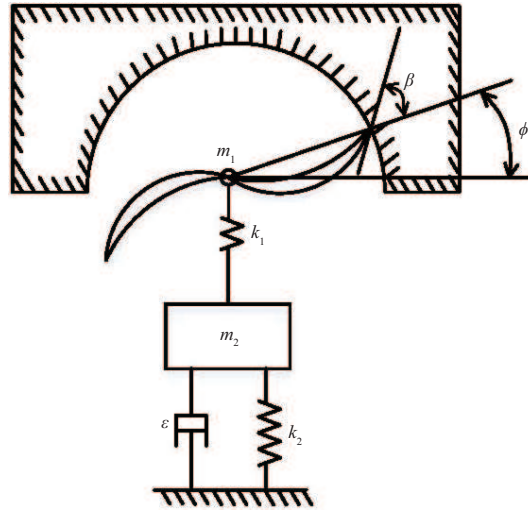
$$\begin{aligned} N_1(\rho) &= -45.7239 + 2.6884\rho, \quad N_{1\tau}(\rho) = -0.2017 + 0.0213\rho, \quad F_1(\rho) = -0.1 - 0.1\rho, \quad M_1 = -1, \\ G_1(\rho) &= \begin{bmatrix} 4.2724 & -0.2 \end{bmatrix} + \begin{bmatrix} -0.2588 & 0 \end{bmatrix} \rho, \quad G_{1\tau}(\rho) = \begin{bmatrix} -0.0098 & -0.02 \end{bmatrix} + \begin{bmatrix} 0.0021 & 0.01 \end{bmatrix} \rho, \quad H_1 = \begin{bmatrix} 0.1 & 0 \end{bmatrix}, \\ N_2(\rho) &= -19.7607 + 0.0355\rho, \quad N_{2\tau}(\rho) = -0.2505 + 0.0125\rho, \quad F_2(\rho) = 0.2\rho, \quad M_2 = 1, \quad H_2 = \begin{bmatrix} 0 & 0.1 \end{bmatrix}, \\ G_2(\rho) &= \begin{bmatrix} -0.1 & -1.9761 \end{bmatrix} + \begin{bmatrix} -0.02 & 0.0035 \end{bmatrix} \rho, \quad G_{2\tau}(\rho) = \begin{bmatrix} -0.01 & -0.0251 \end{bmatrix} + \begin{bmatrix} 0 & -0.0187 \end{bmatrix} \rho. \end{aligned}$$



**Figure 1** (Color online) Case study I: evaluation function with exact-memory when faults  $m_1$  and  $m_2$  occur simultaneously.



**Figure 2** (Color online) Case study I: evaluation function with rough-memory when faults  $m_1$  and  $m_2$  occur simultaneously.



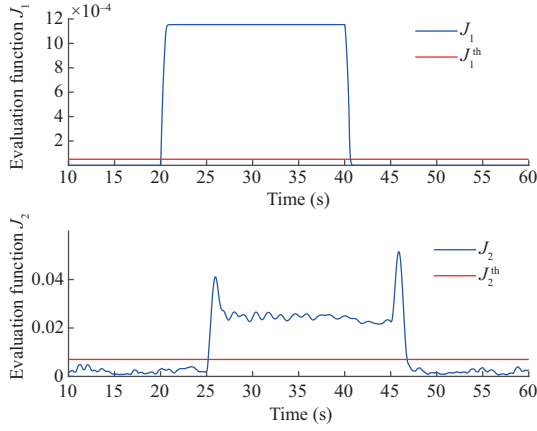
**Figure 3** Case study II: the milling process.

In this situation, we set the length of the evaluation window as  $T_r = 0.9$  s. Accordingly, the threshold values are selected as  $J_1^{\text{th}} = 0.55 \times 10^{-3}$ ,  $J_2^{\text{th}} = 0.6 \times 10^{-3}$ . Figure 2 demonstrates the simulation result when  $m_1$  and  $m_2$  occur simultaneously, which validates the effectiveness of the proposed method with rough-memory.

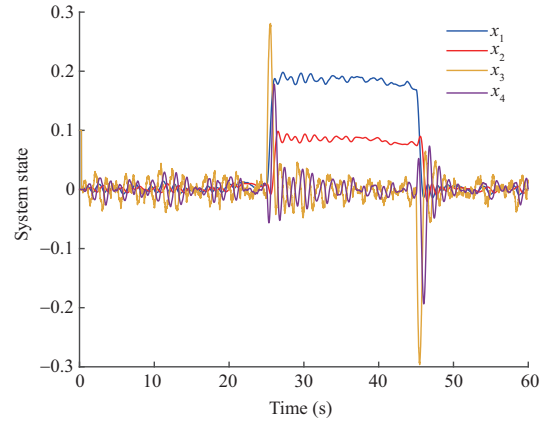
**Remark 10.** The faults considered in the simulation are small compared with disturbance. It can be seen that the proposed geometric approach has good fault diagnosis performance, which shows that it has application potential for the detection of incipient faults. The detection of incipient faults based on the geometric approach is still an open and challenging problem that requires further research.

## 5.2 Case study II

In this subsection, we take an actual system model motivated by the control of chatter during the milling process to further illustrate the FDI performance of the proposed method. As can be seen in Figure 3, the milling machine has two blades that are used to cut material from a workpiece.  $m_1$  and  $m_2$  are the masses of the blade and tool,  $k_1$  and  $k_2$  are the stiffness of the two springs,  $\epsilon$  is the damping coefficient,  $\phi$  is the angular position of the blade, and  $\beta$  depends on the particular material and the used tool. In this simulation,  $\beta$  is set to  $70^\circ$ . For more details of the model, refer to [43, 44]. After making some



**Figure 4** (Color online) Case study II: evaluation function with exact-memory when faults  $m_1$  and  $m_2$  occur simultaneously.



**Figure 5** (Color online) Case study II: system states when faults  $m_1$  and  $m_2$  occur simultaneously.

modifications, we can get the system model as follows:

$$\begin{aligned} \dot{x}(t) &= \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ -10.34 + \rho & 10 & 0 & 0 \\ 5 & -15 & 0 & -0.25 \end{bmatrix} x(t) + \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0.34 - \rho & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} x(t - \tau(t)) + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix} u(t) \\ &+ \begin{bmatrix} 0 \\ 0 \\ -1 \\ 0 \end{bmatrix} d(t) + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix} m_1(t) + \begin{bmatrix} 0 \\ 0 \\ 1 \\ 0 \end{bmatrix} m_2(t), \\ y(t) &= \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} x(t), \end{aligned}$$

where  $\rho = \cos(2\phi + \beta)$ . The time delay  $\tau(t)$  is approximated to be  $\pi/\omega$  where  $\omega$  is the rotation speed of the blade. According to [43], it is assumed that  $\rho \in [-1, 1]$  and  $|\dot{\rho}| \leq 2 \times 1000 \times 2\pi/60$  rad/s,  $\omega \in [200 \times 2\pi/60, 1000 \times 2\pi/60]$  rad/s and  $|\dot{\omega}| = 1000 \times 2\pi/60$  rad/s<sup>2</sup>. The system disturbance is set to  $d(t) = \sin(10t)\delta(t)$  during the simulation period and the initial condition is set to  $[0.1, 0, 0.1, 0]^T$ . In this simulation, we still consider there are two faults which are set as

$$m_1(t) = \begin{cases} 0.1, & 20 \text{ s} < t \leq 40 \text{ s}, \\ 0, & \text{otherwise,} \end{cases} \quad m_2(t) = \begin{cases} 1, & 25 \text{ s} < t \leq 45 \text{ s}, \\ 0, & \text{otherwise.} \end{cases}$$

These two faults exist simultaneously between 25–40 s.

In this case, we consider that the time-delay is exactly known, and the observer matrices can be obtained by verifying the matrix inequalities (15) over a grid of 65 points. The evaluation window is set to  $T_r = 0.5$  s and the threshold values are set to  $J_1^{\text{th}} = 5 \times 10^{-5}$ ,  $J_2^{\text{th}} = 7 \times 10^{-3}$ . The simulation results are shown in Figures 4 and 5. It can be seen from Figure 5 that, compared with fault  $m_2$ , the impact of fault  $m_1$  on the system is very small and almost negligible. However, the proposed method can still effectively achieve the detection and isolation of these two faults, which shows the effectiveness of our method.

## 6 Conclusion

This paper has investigated the FDI problems for state time-delay LPV systems with external disturbance. The core concepts related to the geometric approach, such as invariant subspaces and unobservability subspaces, have been proposed for time-delay LPV systems, and the corresponding calculation algorithms have also been given. The geometric approach has been successfully introduced to the time-delay LPV systems. In this paper, two cases, where the time-delay was known and the time-delay was unknown, have been considered. FDI observers have been designed for both cases based on the geometric approach and  $H_\infty$  techniques, respectively. Wirtinger's inequality has been employed to reduce conservatism when we design the observer matrices. With the proposed geometric FDI observers, fault detection and fault isolation can be performed simultaneously. Finally, simulation examples have been presented to show the validity and effectiveness of the proposed approach. Future research topics include the following aspects: (1) generalizing and applying the geometric approach to other complex systems, such as networked control systems with network-induced delay; (2) investigating better Lyapunov-Krasovskii functionals and inequalities to further reduce conservatism.

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