MOO Paper



Regional Path Moving Horizon Tracking Controller Design for Autonomous Ground Vehicles

Hongyan GUO^{1,2}, Feng LIU², Ru YU², Zhenping SUN³, Hong CHEN^{1,2}*

- State Key Laboratory of Automotive Simulation and Control, Jilin University (Campus NanLing),
 Changchun 130025, PR China;
 - College of Communication Engineering, Jilin University (Campus NanLing),
 Changchun 130025, PR China;
- 3. School of Mechatronic Engineering and Automation, National University of Defense Technology,
 Changsha 410073, PR China





Outline

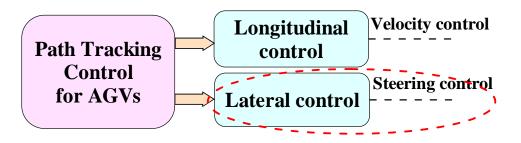
- Introduction
- Regional path tracking problem
- Regional path tracking control
- > Implementation and experiments
- Conclusion





Introduction

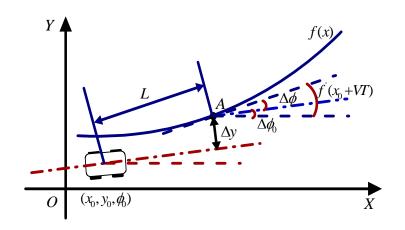
> Path tracking control for AGVs



Steering control:

- > tracks the desired lateral path
- > related to lateral stability

Problems in the existing steering control



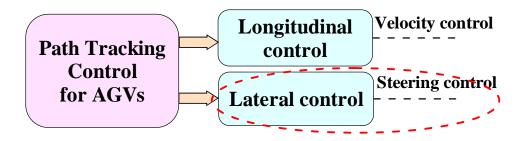
- > road width is ignored
- > vehicle shape is ignored





Introduction

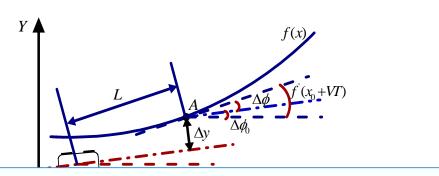
> Path tracking control for AGVs



Steering control:

- > tracks the desired lateral path
- > related to lateral stability

Problems in the existing steering control



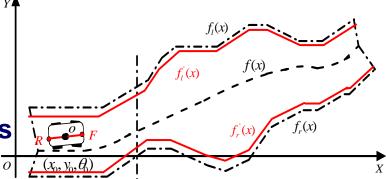
- > road width is ignored
- > vehicle shape is ignored



Control objective:

make control decision repeatedly for AGVs according to the previewed traffic environment and road information, considering the road width and vehicle shape, and keeping AGVs run in the feasible region

- > Regional path tracking problem description
 - \triangleright road boundaries are $f_i(x)$ and $f_r(x)$
 - \succ vehicle is considered as a rectangle with width w and length l
 - keeps vehicle run in the road boundaries
 - \triangleright tracks the centerline f(x)



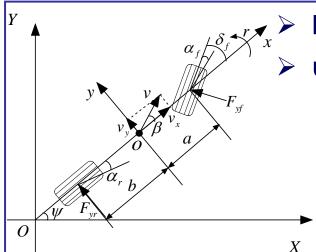
road boundary shrinks $\frac{w}{2}$ vehicle equals to a bar with length l

- Control objective of regional path tracking
 - > keep F and R in the determined region
 - control AGVs travel along the road centerline
 - make driving route as short as possible
 - > consider mechanical characteristics of actuator





Vehicle model

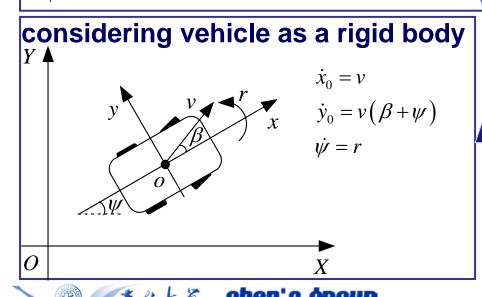


based on the small angle assumption of β and ψ

> using linear tire model $F_{yf} = C_f \alpha_f$, $F_{yr} = C_r \alpha_r$

$$\dot{\beta} = \frac{C_f + C_r}{mv} \beta + \left(\frac{aC_f - bC_r}{mv^2} - 1\right) r - \frac{C_f}{mv} \delta_f$$

$$\dot{r} = \frac{aC_f - bC_r}{I_z}\beta + \frac{a^2C_f + b^2C_r}{I_z v}r - \frac{aC_f}{I_z}\delta_f$$



vehicle could be described as

$$\dot{y}_{o} = v(\psi + \beta)$$

$$\dot{\psi} = r$$

$$\dot{\beta} = \frac{C_{f} + C_{r}}{mv} \beta + \left(\frac{aC_{f} - bC_{r}}{mv^{2}} - 1\right) r - \frac{C_{f}}{mv} \delta_{f}$$

$$\dot{r} = \frac{aC_{f} - bC_{r}}{I_{z}} \beta + \frac{a^{2}C_{f} + b^{2}C_{r}}{I_{z}v} r - \frac{2aC_{f}}{I_{z}} \delta_{f}$$

$$y_{out} = y_{o}$$



Vehicle model

longitudinal velocity is assumed as constant m and I_z varied so slowly that assume as constant C_f and C_r varied so slowly that assume as constant

The vehicle model could be treated as linear-time-invariant system

$$\dot{x} = Ax + Bu$$

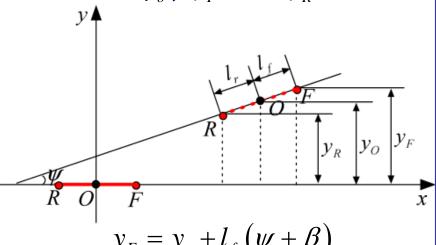
$$y_{out} = Cx$$

$$A = \begin{bmatrix} 0 & v & v & 0 \\ 0 & 0 & 0 & 1 \\ 0 & 0 & \frac{C_f + C_r}{mv} & \frac{aC_f - bC_r}{mv^2} - 1 \\ 0 & 0 & \frac{aC_f - bC_r}{I_z} & \frac{a^2C_f + b^2C_r}{I_zv} \end{bmatrix} \qquad B = \begin{bmatrix} 0 \\ 0 \\ -\frac{C_f}{mv} \\ -\frac{aC_f}{I_z} \end{bmatrix} \qquad C = \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{bmatrix}^T \qquad x = [y \quad \phi \quad \beta \quad r]$$



According to the relationship

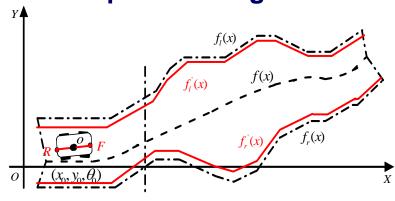
between y_o , y_F and y_R



$$y_F = y_o + l_f (\psi + \beta)$$

$$y_R = y_o - l_r (\psi + \beta)$$

lateral positions of front and rear end keeps in the region



$$f_l(x) \le y_F \le f_r(x)$$

$$f_l(x) \le y_R \le f_r(x)$$

The front and rear end in the region could be transformed into the constraints of lateral position

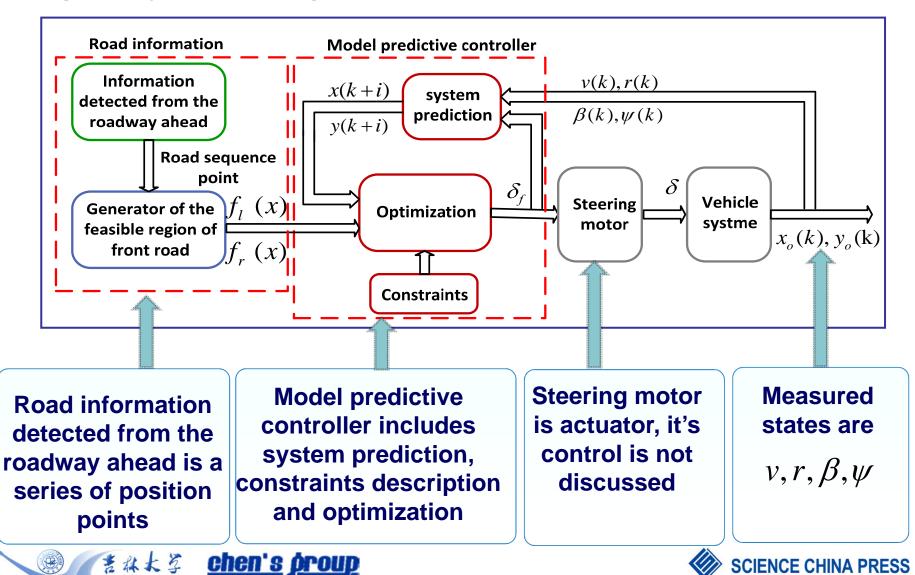
$$f_r'(x) - l_f(\beta + \psi) \le y \le f_l'(x) - l_f(\beta + \psi)$$

$$f_{r}(x) + l_{r}(\beta + \psi) \le y \le f_{l}(x) + l_{r}(\beta + \psi)$$





Regional path tracking control scheme

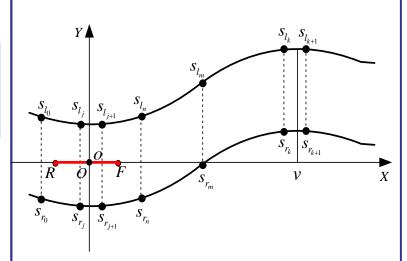


Road information processing

$$\begin{cases} f_r(x) = \sum \prod_{i \neq p} \frac{(x - x_r(i))}{(x_r(p) - x_r(i))} y_r(p) & p = j, n, m, k; \\ f_l(x) = \sum \prod_{i \neq p} \frac{(x - x_l(i))}{(x_l(p) - x_l(i))} y_l(p) & i = j, n, m, k. \end{cases}$$

- > road point sequence (x_r, y_r, x_l, y_l) is obtained from perception system
- j,n,m,k: four sets of interpolation points position chosen from given road points
- four sets of interpolation points equally spaced
- interpolation points are selected based on quadratic search algorithm

$$n = \left\lfloor \frac{k-j}{3} \right\rfloor + j, \quad m = \left\lfloor \frac{k-j}{3} \right\rfloor + n$$



 \checkmark first time: find start point (s_{r_i}, s_{l_i})

$$\begin{cases} x_r(j) \cdot x_r(j+1) \le 0 \\ x_l(j) \cdot x_l(j+1) \le 0 \end{cases}$$

 \checkmark second time: find final point (s_{r_k}, s_{l_k})

$$\begin{cases} (x_r(k) - v) \cdot (x_r(k+1) - v) \le 0 \\ (x_l(k) - v) \cdot (x_l(k+1) - v) \le 0 \end{cases}$$

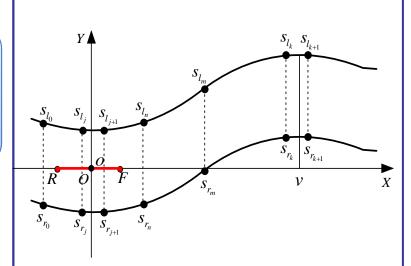




Road information processing

$$\begin{cases} f_r(x) = \sum \prod_{i \neq p} \frac{(x - x_r(i))}{(x_r(p) - x_r(i))} y_r(p) & p = j, n, m, k; \\ f_l(x) = \sum \prod_{i \neq p} \frac{(x - x_l(i))}{(x_l(p) - x_l(i))} y_l(p) & i = j, n, m, k. \end{cases}$$

- > road point sequence (x_r, y_r, x_l, y_l) is obtained from perception system
- j, n, m, k: four sets of interpolation points position chosen from given road points
- four sets of interpolation points equally spaced



 \checkmark first time: find start point (s_{r_i}, s_{l_i})

$$\int x_r(j) \cdot x_r(j+1) \le 0$$

When the road boundary is determined, the road centerline could be obtained

$$f(x) = \frac{1}{2} (f_l(x) + f_r(x))$$

_ 3 _

3

 $(x_l(k) - v) \cdot (x_l(k+1) - v) \le 0$





Moving horizon controller design

> Vehicle system dynamic prediction

By discretizing the continuous-time model, the system is described as

$$x(k+1) = A_c x(k) + B_c u(k)$$
$$y_c(k) = C_c x(k)$$

Define road centerline as reference input

$$R(k) = \lceil f(k) \quad f(k+1) \quad \cdots \quad f(k+P-1) \rceil$$

Define the predicted input and output sequence

$$U(k) = \begin{bmatrix} u(k) \\ u(k+1) \\ \vdots \\ u(k+N-1) \end{bmatrix}$$

$$Y(k+1|k) = \begin{bmatrix} y(k+1) \\ y(k+2) \\ \vdots \\ y(k+P) \end{bmatrix}$$

Control objective description

objective 1: runs along the centerline

$$J_1 = ||Y(k+1|k) - R(k)||^2$$

objective 2: minimize driving route

$$J_{2} = \sum_{i=1}^{P} \left(\left\| \Delta x_{d} (k+i) \right\|^{2} + \left\| \Delta y_{d} (k+i) \right\|^{2} \right)$$

objective 3: control action is limited

 $J_3 = ||U(k)||^2$ objective 4: vehicle runs in the region

$$U(k) = \begin{bmatrix} u(k) \\ u(k+1) \\ \vdots \\ u(k+N-1) \end{bmatrix}$$

$$0bjective 4 : vehicle runs in the region$$

$$\begin{cases} f_r'(k+i) - l_f(\psi(k+i) + \beta(k+i)) \le y_o(k+i) \le f_l'(k+i) - l_f(\psi(k+i) + \beta(k+i)) \\ f_r'(k+i) + l_r(\psi(k+i) + \beta(k+i)) \le y_o(k+i) \le f_l'(k+i) + l_r(\psi(k+i) + \beta(k+i)) \end{cases}, i = 1, \dots, P$$

objective 5: steering actuator saturation

$$\begin{cases} \left| \delta_{f}(k+i) \right| \leq \delta_{fsat} \\ \left| \Delta \delta_{f}(k+i) \right| \leq \Delta \dot{\delta}_{fsat} \cdot T_{s} \end{cases}, i = 0, \dots, N-1$$



Moving horizon controller design

> Vehicle system dynamic prediction

By discretizing the continuous-time model, the system is described as

$$x(k+1) = A_c x(k) + B_c u(k)$$
$$y_c(k) = C_c x(k)$$

Define road centerline as reference input

$$R(k) = \lceil f(k) \quad f(k+1) \quad \cdots \quad f(k+P-1) \rceil$$

Define the predicted input and output sequence !

> Control objective description

objective 1: runs along the centerline

$$J_1 = ||Y(k+1|k) - R(k)||^2$$

objective 2: minimize driving route

$$J_{2} = \sum_{i=1}^{P} \left(\left\| \Delta x_{d} (k+i) \right\|^{2} + \left\| \Delta y_{d} (k+i) \right\|^{2} \right)$$

objective 3: control action is limited

$$J_3 = \left\| U\left(k\right) \right\|^2$$

Minimize these three objectives simultaneously is contradictive, weighting factors are introduced. The multi-objective function could be obtained as

$$J = \left\| \Gamma_{y} (Y(k+1|k) - R(k)) \right\|^{2} + \left\| \Gamma_{u} U(k) \right\|^{2} + \sum_{i=1}^{P} \Gamma_{d,i} \left(\left\| \Delta x_{d} (k+i) \right\|^{2} + \left\| \Delta y_{d} (k+i) \right\|^{2} \right)$$

$$Y(k+1|k) = \begin{bmatrix} y(k+2) \\ \vdots \\ y(k+P) \end{bmatrix}$$

$$\begin{cases} \left| \delta_{f}(k+i) \right| \leq \delta_{fsat} \\ \left| \Delta \delta_{f}(k+i) \right| \leq \Delta \dot{\delta}_{fsat} \cdot T_{s} \end{cases}, i = 0, \dots, N-1$$





Optimization problem description

$$\min_{U(k)} J = \left\| \Gamma_{y}(Y(k+1|k) - R(k)) \right\|^{2} + \left\| \Gamma_{u}U(k) \right\|^{2} + \sum_{i=1}^{P} \Gamma_{d,i} \left(\left\| \Delta x_{d} \left(k+i \right) \right\|^{2} + \left\| \Delta y_{d} \left(k+i \right) \right\|^{2} \right)$$
Subject to:
$$x(k+i+1) = A_{c}x(k+i) + B_{c}\delta_{f}(k+i) + B_{dc}d(k+i)$$

$$y_{o} = C_{c}x(k+i)$$

$$f'_{r}(k+i) - l_{f}(\psi(k+i) + \beta(k+i)) \leq y_{o}(k+i) \leq f'_{l}(k+i) - l_{f}(\psi(k+i) + \beta(k+i))$$

$$f'_{r}(k+i) + l_{r}(\psi(k+i) + \beta(k+i)) \leq y_{o}(k+i) \leq f'_{l}(k+i) + l_{r}(\psi(k+i) + \beta(k+i))$$

$$\left| \delta_{f}(k+i) \right| \leq \delta_{fsat}$$

$$\left| \Delta \delta_{f}(k+i) \right| \leq \Delta \dot{\delta}_{fsat} \cdot T_{s}$$

The related matrices and variables could be computed as

$$A_{c} = e^{AT_{s}}, \quad B_{c} = \int_{0}^{T_{s}} e^{A\tau} d\tau \cdot B, \quad B_{dc} = B_{d} \quad C_{c} = C$$

$$\Delta x_{d} (k+i) = v(k) \cdot T_{s}, \quad \Delta y_{d} (k+i) = y_{o} (k+i) - y_{o} (k+i)$$

$$\Delta \delta_{f} (k+i) = \delta_{f} (k+i) - \delta_{f} (k+i-1)$$

Only the first element U(k) is applied to the vehicle





Implementation and experiments

Implementation

- > MPC algorithm is implemented based on C language
- > differential evolution is employed to solve the optimization
- Experiment setup
 - > vehicle: Hongqi vehicle HQ430
 - > sensor: OTXS RT3002 and 2 cameras
 - experimental system: VxWorks and Windows
 - > tools: Visual Studio 2010 and Tornado2.2
 - > computers: 2 Thinkpad T420







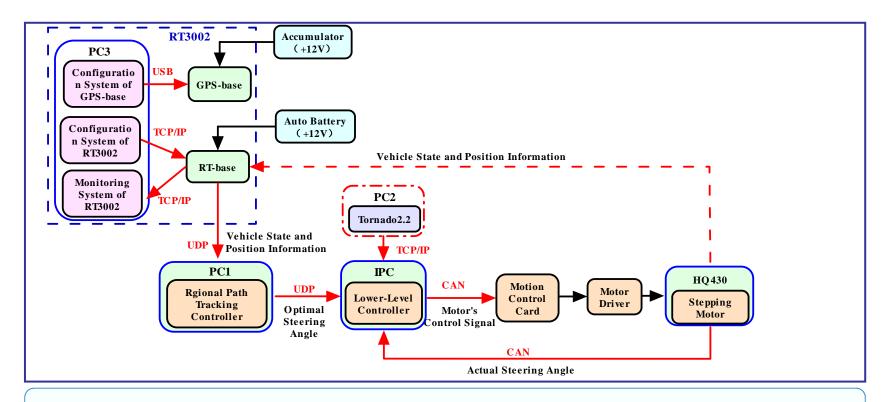






Implementation and experiments

communication system used in experiments



RT3002 regional path tracking controller : UDP

Regional path tracking controller driving control system: UDP

Driving control system steering motor: CAN

Hongqi AGV driving control system and RT3002: CAN





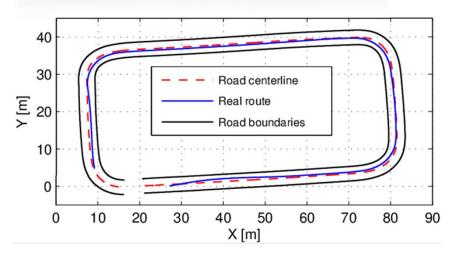


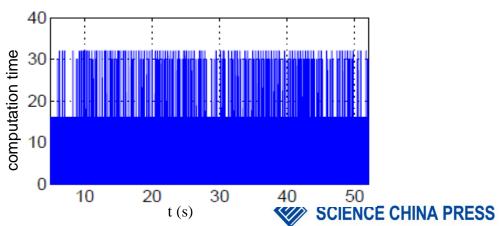
Implementation and experiments

> experiments result









Conclusions

- > A novel description of AGVs' path tracking issue is proposed
- Regional path moving horizon control is presented
- Road perception information is processed
- Experiments are carried out based on Hongqi AGV HQ430
- > Effectiveness of the proposed method is verified







Thank you