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输入死区下的多输入多输出系统自适应神经网络容错控制

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摘要 针对一类具有传感器故障和不对称输入死区的非线性多输入多输出非严格反馈系统,本文提出一种自适应神经网络容错控制方案.控制器的设计以反步法为框架,采用自适应神经网络控制方法处理传感器故障,利用死区斜率的有界性补偿输入死区对系统性能造成的影响,同时引入动态面控制技术克服"计算爆炸"的问题.该控制方法不仅能够保证闭环系统中所有信号半全局一致最终有界,而且能使跟踪误差收敛至原点附近的紧集内.最后通过两个仿真实验验证该控制方法的有效性.

关键词 非线性系统, 传感器故障, 容错控制, 动态面控制, 输入死区

1 引言

近年来,反步法已成为非线性系统控制设计的有效工具,对非线性系统控制理论的发展起着重要的作用^[1~3].自适应反步法属于系统化的递归式设计方法,在反步法的基础上引入自适应律,解决了在线估计系统中的未知参数问题^[4].在自适应反步法的框架之下,研究者可以利用神经网络或模糊逻辑系统逼近系统模型中的未知非线性函数,进而设计出使系统稳定的控制器^[5].然而,自适应反步法仍然存在某些不足之处.例如,在设计控制器的过程中,需要对虚拟控制器进行反复求导,从而增加了计算负担,出现"计算爆炸"的问题.Tong 等^[6]在反步法设计过程中结合动态面控制技术克服了此类问题.

多输入多输出非线性系统具有并行传送数据的特点,且广泛存在于实际工程中.借助于反步法和 神经网络,研究者们极大地推进了多输入多输出非线性系统控制理论的发展^[7~9]. Chen 等^[7]研究了

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 Zhou Q, Lin G H, Ma H, et al. Adaptive neural network fault-tolerant control for MIMO systems with dead zone inputs (in Chinese). Sci Sin Inform, 2021, 51: 618-632, doi: 10.1360/SSI-2019-0198

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一类鲁棒自适应控制问题,为分析具有输入饱和与输入死区的多输入多输出严格反馈系统提供了新的 思路.针对含有控制方向未知的多输入多输出系统,Zhou 等^[8]结合 Nussbaum 函数,提出了一种新颖 的自适应神经网络控制方法.值得注意的是,虽然上述研究为非线性系统控制器设计提供了有效的途 径,但并不适用于非严格反馈形式下的非线性系统.

非严格反馈形式是一种常见的非线性系统形式.对于非线性非严格反馈系统,由于系统中的非线性函数包含全状态变量,在设计控制器时会产生代数环问题.因此,为了解决非严格反馈所带来的上述问题,Chen 等^[10]和 Wang 等^[11]应用变量分离的方法,统一在反步法的最后一步处理状态分离后的非线性函数,而 Li 等^[12]和 Ma 等^[13]利用模糊基函数的性质对非线性函数进行变换,最终设计出可以保证系统稳定的自适应模糊控制器.与上述文献不同的是,Wang 等^[14]和 Sun 等^[15]利用径向基神经网络的性质改变基函数向量的状态,使控制器的设计过程更为简洁直观.虽然学者们在非线性系统自适应控制的研究方面已经取得了许多成果,但对于实际应用中传感器故障和输入死区同时出现的情况,往往没有进行充分的考虑与分析.

事实上,随着现代科学技术的飞速发展,工业过程控制系统的规模和复杂度都在不断增加,系统 一旦发生故障, 轻则降低系统性能, 重则破坏系统稳定性, 造成不可预估的损失 [16~20]. 因此, 提高控 制系统的可靠性和安全性显得尤为关键,而容错控制的出现和发展有效地解决了此类问题.对于发生 传感器故障的系统,许多学者提出了有效的自适应主动容错控制方法,通过适当调整控制器的参数来 补偿故障,进而减小传感器故障对系统的影响^[21~23]. Yan 等^[24] 基于滑模观测器提出了一种故障重 构方法,利用重构信号逼近故障信号,从而使故障检测与诊断方法的实用性更强.针对一类具有传感 器故障的二阶多输入多输出非线性系统, Khebbache 等^[25]设计了一种基于自适应动态面控制方法的 容错控制器, Bounemeur 等^[26] 基于模糊逻辑系统提出了一种自适应模糊容错控制方法. Zhang 等^[27] 设计了一种包含自适应故障补偿机制的控制器,解决了传感器部分失效故障的问题,另一方面,输入 死区作为一种非光滑的非线性特性,若在容错控制设计中忽视其存在,可能会严重地影响系统的控制 性能,为了使具有死区的非线性系统保持稳定性,许多学者对此提出了多种自适应控制方法^[28~30].Li 等^[31] 基于模糊逼近理论,利用死区斜率的有界性解决了输入死区问题. Luo 等^[32] 基于自适应反步 法提出了一种补偿执行器死区的容错控制方法. 针对一类具有未知死区和执行器故障的不确定非线 性互联大系统, Chen 等^[33]设计了一种自适应神经网络容错控制器.鉴于对以上文献的分析, 在容错 控制设计的过程中考虑输入死区对系统的影响是非常有必要的.因此,本文针对一类具有传感器故障 和不对称输入死区的非线性多输入多输出非严格反馈系统,提出了一种新的自适应神经网络容错控制 方法.

本文的主要贡献如下: (1) 相比文献 [25,26], 本文考虑了 m 阶多输入多输出系统, 更具有一般 性. 与此同时, 本文考虑的 m 阶非线性系统还受输入死区影响, 在不需要建立死区逆模型的情况下, 我们利用死区斜率的有界性补偿不对称死区非线性的问题. (2) 与文献 [10,11] 不同的是, 本文不需要 文献 [10,11] 中对非线性函数的假设, 从而降低了设计的保守性, 并使控制器的设计过程更简单直接. (3) 该控制方法将未知神经网络权重向量作为估计参数, 减少了自适应参数的数量, 有效地降低了计算 负担.

本文的后续部分安排如下:第2节介绍了文章的系统,并阐述了传感器故障和输入死区的问题; 第3节介绍了自适应神经网络控制器的设计和相应的稳定性分析;第4节采用两个仿真实验对所提 出的控制方法进行验证;第5节对全文进行总结.



图 1 传感器故障类型示意图 Figure 1 Types of sensor faults

2 问题阐述

考虑一类具有非严格反馈形式的多输入多输出非线性系统:

$$\dot{x}_{j,i} = f_{j,i}(x) + x_{j,i+1},
\dot{x}_{j,m} = f_{j,m}(x) + u_j,
y_j = h(x_{j,1}),$$
(1)

其中, $j = 1, 2, ..., n, i = 1, 2, ..., m - 1, x = [x_1^T, x_2^T, ..., x_n^T]^T, x_j = [x_{j,1}, x_{j,2}, ..., x_{j,m}]^T \in \mathbb{R}^m, y_j$ 为 第 j 个子系统的输出, $u_j \in \mathbb{R}$ 为第 j 个子系统的输入, $f_{j,i}(\cdot)$ 为未知光滑非线性函数, 且满足 $f_{j,i}(0) = 0$. 系统的传感器故障模型为: $h(x_{j,1}) = K_j x_{j,1} + q_j(t)$, 其中, K_j 和 $q_j(t)$ 为传感器故障的参数, 且满足 以下条件: $0 < \bar{K}_{j,\min} \leq K_j \leq 1, -\bar{q}_j \leq q_j(t) \leq \bar{q}_j$. $\bar{K}_{j,\min}$ 表示传感器最小影响值, \bar{q}_j 与 $-\bar{q}_j$ 分别表 示 $q_j(t)$ 的上界与下界. 传感器故障示意图如图 1 所示, 且故障类型总结如下:

(1) 当 $K_j = 1$, $q_j(t)$ 为常数, 传感器发生偏差故障; (2) 当 $K_j = 1$, $|q_j(t)| = \varphi t$, $0 < \varphi \ll 1$, 传感器 发生漂移故障; (3) 当 $K_j = 1$, $|q_j(t)| < \bar{q}_j$, $q_j(t) \to 0$, 传感器发生精度下降故障; (4) 当 $0 < \bar{K}_{j,\min} \leq K_i < 1$, $q_i(t) = 0$, 传感器发生失效故障.

令 $f_{sj} = (K_j - 1)x_{j,1} + q_j(t)$, 其中 $f_{sj} \in \mathbb{R}$ 表示传感器故障向量, 且 $y_j = x_{j,1} + f_{sj}$. y_j 的导数 为 $\dot{y}_j = \dot{x}_{j,1} + f_{psj}$. 其中, $\dot{f}_{sj} = f_{psj}$. u_j 是一个不对称输入死区非线性函数, 定义如下:

$$u_{j} = D_{j}(\varpi_{j}) \triangleq \begin{cases} o_{jr}(\varpi_{j} - p_{jr}), & \varpi_{j} \ge p_{jr}, \\ 0, & -p_{jl} < \varpi_{j} < p_{jr}, \\ o_{jl}(\varpi_{j} + p_{jl}), & \varpi_{j} \le -p_{jl}. \end{cases}$$
(2)

不对称死区非线性函数如图 2 所示, $\varpi_j \in \mathbb{R}$ 表示第 *j* 个死区的输入, o_{jl} 和 o_{jr} 分别表示死区特性的左斜率和右斜率, p_{jl} 和 p_{jr} 分别表示左断点和右断点.

假设1 ([29]) 存在一个大于 0 的常数 M_m 满足: $|\varpi_j| \leq M_m$, 其中 j = 1, 2, ..., n.



图 2 不对称死区非线性函数 Figure 2 Nonsymmetric dead-zone nonlinearity

假设2 ([29]) 参数 o_{jr} , o_{jl} , p_{jr} , p_{jl} 均为大于 0 的常数, 且 $o_{jr} \neq o_{jl}$. 将式 (2) 改写为

$$u_j = o_j(t)\varpi_j(t) + \lambda_j(t), \tag{3}$$

其中,

$$o_j(t) = \begin{cases} o_{jl}, & \varpi_j \leq 0, \\ o_{jr}, & \varpi_j > 0, \end{cases}$$

$$\tag{4}$$

$$\lambda_{j}(t) = \begin{cases} -o_{jr}p_{jr}, & \varpi_{j} \ge p_{jr}, \\ -o_{j}(t)\varpi_{j}(t), & -p_{jl} < \varpi_{j} < p_{jr}, \\ o_{jl}p_{jl}, & \varpi_{j} \leqslant -p_{jl}. \end{cases}$$
(5)

由式 (5) 可得

$$\lambda_j(t) \leqslant \bar{\lambda}_j, \quad \bar{\lambda}_j = \max\{o_{jl} p_{jl}, o_{jr} p_{jr}\}.$$
(6)

 $\mathbb{E} \ X \ \bar{\alpha}_j = \max\{o_{jl}, o_{jr}\}, \ \underline{\alpha}_j = \min\{o_{jl}, o_{jr}\},$

$$\frac{o_j(t)}{\underline{\alpha}_j} = 1 + \rho_j(t),\tag{7}$$

其中, $\rho_j(t) \ge 0$. 由式 (4) 和 (7) 得

$$\rho_j(t) \leqslant \frac{\bar{\alpha}_j}{\underline{\alpha}_j} - 1. \tag{8}$$

将式 (7) 代入式 (3) 可得,

$$u_j = \underline{\alpha}_j (1 + \rho_j(t)) \overline{\omega}_j(t) + \lambda_j(t).$$
(9)

假设3 ([8]) 对于 j = 1, 2, ..., n, 参考信号 y_{dj} 与其 m 阶导数均是连续有界的. 假设给定一个大于 0 的常数 ε , 对于任意的连续函数 $f(\zeta)$, 存在一个神经网络 $W^{T}S(\zeta)$ 使得

 $f(\zeta) = W^{\mathrm{T}}S(\zeta) + \delta(\zeta), \quad |\delta(\zeta)| \leq \varepsilon,$

其中, 理想权重向量 $W = [w_1, w_2, \dots, w_{\iota}]^T \in \mathbb{R}^{\iota}$, 且 $\iota > 1, \iota$ 表示神经网络的节点数, ζ 表示输入向量, 且 $\forall \zeta \in \Omega_{\zeta} \subset \mathbb{R}^n$, $S(\zeta) = [S_1(\zeta), S_2(\zeta), \dots, S_{\iota}(\zeta)]^T$ 代表高斯 (Gauss) 函数向量组, 且

$$S_j(\zeta) = \exp\left[\frac{-(\zeta - \mu_j)^{\mathrm{T}}(\zeta - \mu_j)}{\Phi_j^2}\right], \quad j = 1, 2, \dots, \iota,$$

其中, $\mu_j = [\mu_{j1}, \mu_{j2}, \dots, \mu_{jn}]^T$ 表示可取范围的中心, Φ_j 为高斯函数的宽度.

引理1 ([14]) 定义 $\bar{x}_{j,q} = [x_{j,1}, x_{j,2}, \dots, x_{j,q}]^{\mathrm{T}}$,其中 $S_j(\bar{x}_{j,q}) = [S_{j,1}(\bar{x}_{j,q}), S_{j,2}(\bar{x}_{j,q}), \dots, S_{j,m}(\bar{x}_{j,q})]^{\mathrm{T}}$ 为神经网络的基函数向量.对于任意正数 $p \leq q$,以下不等式成立:

$$||S_j(\bar{x}_{j,q})||^2 \leq ||S_j(\bar{x}_{j,p})||^2.$$

3 主要结果

基于反步法和动态面控制技术,本文设计一种自适应神经网络容错控制器和自适应律,使得闭环 系统的所有信号都是半全局一致最终有界,并使跟踪误差收敛到零的小邻域内.

在 m 步的反步设计过程中, 每一步都基于以下的坐标变换:

$$z_{j,1} = y_j - y_{dj},$$

$$z_{j,i} = x_{j,i} - \alpha_{j,i,f},$$

$$\chi_{j,i} = \alpha_{j,i,f} - \alpha_{j,i-1}$$

其中, $j = 1, 2, ..., n, i = 2, 3, ..., m, z_{j,1}$ 为跟踪误差, $z_{j,i}$ 为误差面, $x_{j,i}$ 为状态变量, $\chi_{j,i}$ 为一阶滤波器的输出误差, $\alpha_{j,i-1}$ 和 $\alpha_{j,i,f}$ 分别表示虚拟控制器信号和滤波器输出信号.

定义未知常数 θ_j 和 Θ_j 为: $\theta_j = \max\{||W_{j,i}||^2\}$ 和 $\Theta_j = ||W_{psj}||^2$,其中,i = 1, 2, ..., m. 第 j, 1 步的虚拟控制器 $\alpha_{j,1}$ 和自适应律 $\hat{\Theta}_j$ 为

$$\alpha_{j,1} = -k_{j,1}z_{j,1} - z_{j,1} - \frac{1}{2c_{j,1}^2}z_{j,1}\hat{\theta}_j S^{\mathrm{T}}(Y_{j,1})S(Y_{j,1}) - \frac{1}{2c_{psj}^2}z_{j,1}\hat{\Theta}_j S_{psj}^{\mathrm{T}}(\zeta_{psj})S_{psj}(\zeta_{psj}), \qquad (10)$$

$$\dot{\hat{\Theta}}_j = \frac{\beta_j}{2c_{psj}^2} z_{j,1}^2 S_{psj}^{\mathrm{T}}(\zeta_{psj}) S_{psj}(\zeta_{psj}) - d_j \hat{\Theta}_j,$$
(11)

其中, j = 1, 2, ..., n, $Y_{j,1} = [x_{j,1}, \dot{y}_{dj}]^{\mathrm{T}}$, $\zeta_{psj} = x_{psj}^{\mathrm{T}}$, $k_{j,1}$, $c_{j,1}$, c_{psj} , β_j , d_j 均为大于 0 的常数. $\hat{\theta}_j \notin \theta_j$ 的估计, $\hat{\Theta}_j \notin \Theta_j$ 的估计.

第 j, i步的虚拟控制器 $\alpha_{j,i}$ 为

$$\alpha_{j,i} = -k_{j,i} z_{j,i} - z_{j,i-1} - \frac{1}{2} z_{j,i} - \frac{1}{2c_{j,i}^2} z_{j,i} \hat{\theta}_j S^{\mathrm{T}}(Y_{j,i}) S(Y_{j,i}), \qquad (12)$$

其中, $i = 2, \ldots, m - 1, c_{j,i} > 0, k_{j,i} > 0, Y_{j,i} = \bar{x}_{j,i}$. 此外, $\bar{x}_{j,i} = [x_{j,1}, x_{j,2}, \ldots, x_{j,i}]^{\mathrm{T}} \in \mathbb{R}^{i}$ 为系统中的 第 j 个子系统的状态向量.

第 j,m步的控制器 $\varpi_j(t)$ 和自适应律 $\hat{\theta}_j$ 为

$$\overline{\omega}_{j}(t) = -\frac{1}{\underline{\alpha}_{j}} \left[k_{j,m} z_{j,m} + \frac{1}{2} z_{j,m} + z_{j,m-1} + \frac{1}{2c_{j,m}^{2}} z_{j,m} \hat{\theta}_{j} S^{\mathrm{T}}(Y_{j,m}) S(Y_{j,m}) \right] - \frac{1}{\underline{\alpha}_{j}} (\bar{\alpha}_{j} - \underline{\alpha}_{j}) M_{m}, \quad (13)$$

$$\dot{\hat{\theta}}_{j} = \sum_{i=1}^{m} \frac{r_{j}}{2c_{j,i}^{2}} z_{j,i}^{2} S^{\mathrm{T}}(Y_{j,i}) S(Y_{j,i}) - b_{j} \hat{\theta}_{j}, \quad (14)$$

 $\label{eq:expansion} \begin{tabular}{lll} \begin$

步骤 j,1 选取 Lyapunov 函数为

$$V_{j,1} = \frac{1}{2}z_{j,1}^2 + \frac{1}{2r_j}\tilde{\theta}_j^2 + \frac{1}{2\beta_j}\tilde{\Theta}_j^2,$$

其中, $\tilde{\theta}_j = \theta_j - \hat{\theta}_j$, $\tilde{\Theta}_j = \Theta_j - \hat{\Theta}_j$. 对 $V_{j,1}$ 求导, 其导数为

$$\dot{V}_{j,1} = z_{j,1}(\bar{f}_{j,1}(\zeta_{j,1}) + \alpha_{j,1}) + z_{j,1}(\alpha_{j,2,f} - \alpha_{j,1}) + z_{j,1}z_{j,2} + z_{j,1}f_{psj} - \frac{1}{r_j}\tilde{\theta}_j\dot{\hat{\theta}}_j - \frac{1}{\beta_j}\tilde{\Theta}_j\dot{\hat{\Theta}}_j, \quad (15)$$

其中, $\zeta_{j,1} = [x^{\mathrm{T}}, \dot{y}_{dj}]^{\mathrm{T}}, \bar{f}_{j,1}(\zeta_{j,1}) = f_{j,1} - \dot{y}_{dj}$. 通过使用神经网络, 对系统中的未知非线性函数 $\bar{f}_{j,1}(\zeta_{j,1})$ 和 $f_{psj}(\zeta_{psj})$ 进行逼近, 如下所示

$$\bar{f}_{j,1}(\zeta_{j,1}) = W_{j,1}^{\mathrm{T}}S(\zeta_{j,1}) + \delta_{j,1}(\zeta_{j,1}),$$

其中, $|\delta_{j,1}| \leq \varepsilon_{j,1}$, 且 $\varepsilon_{j,1} > 0$. 使用引理 1 和 Young's 不等式, 可得

$$z_{j,1}\bar{f}_{j,1}(\zeta_{j,1}) = z_{j,1}(W_{j,1}^{\mathrm{T}}S(\zeta_{j,1}) + \delta_{j,1}(\zeta_{j,1}))$$

$$\leqslant \frac{1}{2}z_{j,1}^{2} + \frac{1}{2}c_{j,1}^{2} + \frac{1}{2}\varepsilon_{j,1}^{2} + \frac{1}{2}c_{j,1}^{2}z_{j,1}^{2}\theta_{j}S^{\mathrm{T}}(Y_{j,1})S(Y_{j,1}),$$
(16)

其中, $Y_{j,1} = [x_{j,1}, \dot{y}_{dj}]^{\mathrm{T}}$. 类似地, $f_{psj}(\zeta_{psj}) = W_{psj}^{\mathrm{T}}S_{psj}(\zeta_{psj}) + \delta_{psj}(\zeta_{psj})$, 其中, $|\delta_{psj}| \leq \varepsilon_{psj}$, 且 $\varepsilon_{psj} > 0$. 使用 Young's 不等式, 可得

$$z_{j,1}f_{psj} = z_{j,1}(W_{psj}^{\mathrm{T}}S_{psj}(\zeta_{psj}) + \delta_{psj}(\zeta_{psj}))$$

$$\leqslant \frac{1}{2}z_{j,1}^{2} + \frac{1}{2}c_{psj}^{2} + \frac{1}{2}\varepsilon_{psj}^{2} + \frac{1}{2}c_{psj}^{2}z_{j,1}^{2}\Theta_{j}S_{psj}^{\mathrm{T}}(\zeta_{psj})S_{psj}(\zeta_{psj}), \qquad (17)$$

其中, ζ_{psj} = x_{psj}. 将式 (16) 和 (17) 代入式 (15), 根据式 (10) 和 (11), 可得

$$\dot{V}_{j,1} \leqslant -k_{j,1}z_{j,1}^{2} + \frac{1}{2c_{j,1}^{2}}z_{j,1}^{2}\tilde{\theta}_{j}S^{\mathrm{T}}(Y_{j,1})S(Y_{j,1}) + \frac{1}{2c_{psj}^{2}}z_{j,1}^{2}\tilde{\Theta}_{j}S_{psj}^{\mathrm{T}}(\zeta_{psj})S_{psj}(\zeta_{psj}) + \frac{1}{2}c_{j,1}^{2} \\
+ \frac{1}{2}\varepsilon_{j,1}^{2} + \frac{1}{2}c_{psj}^{2} + \frac{1}{2}\varepsilon_{psj}^{2} - \frac{1}{r_{j}}\tilde{\theta}_{j}\dot{\theta}_{j} + z_{j,1}z_{j,2} - \frac{1}{\beta_{j}}\tilde{\Theta}_{j}\dot{\Theta}_{j} + z_{j,1}(\alpha_{j,2,f} - \alpha_{j,1}) \\
\leqslant -k_{j,1}z_{j,1}^{2} + z_{j,1}z_{j,2} + \frac{1}{2}c_{j,1}^{2} + \frac{1}{2}c_{psj}^{2} + \frac{1}{2}\varepsilon_{psj}^{2} + \frac{1}{2}\varepsilon_{psj}^{2} + \frac{1}{2}\varepsilon_{j,1}^{2} Z_{j,1}^{2}S^{\mathrm{T}}(Y_{j,1})S(Y_{j,1}) - \dot{\theta}_{j} \\
+ \frac{1}{2}\varepsilon_{j,1}^{2} + z_{j,1}(\alpha_{j,2,f} - \alpha_{j,1}) + \frac{d_{j}}{\beta_{j}}\tilde{\Theta}_{j}\hat{\Theta}_{j}.$$
(18)

对 $\frac{d_j}{\beta_i} \tilde{\Theta}_j \hat{\Theta}_j$ 使用 Young's 不等式放缩, 可得

$$\frac{d_j}{\beta_j}\tilde{\Theta}_j\hat{\Theta}_j \leqslant -\frac{d_j}{2\beta_j}\tilde{\Theta}_j^2 + \frac{d_j}{2\beta_j}\Theta_j^2.$$
(19)

将式 (19) 代入式 (18), 可得

$$\dot{V}_{j,1} \leqslant -k_{j,1}z_{j,1}^2 + z_{j,1}z_{j,2} + \frac{1}{r_j}\tilde{\theta}_j \left[\frac{r_j}{2c_{j,1}^2} z_{j,1}^2 S^{\mathrm{T}}(Y_{j,1}) S(Y_{j,1}) - \dot{\hat{\theta}}_j \right] + z_{j,1}(\alpha_{j,2,f} - \alpha_{j,1}) + \Xi_{j,1} - \frac{d_j}{2\beta_j}\tilde{\Theta}_j^2,$$

其中, $\Xi_{j,1} = \frac{1}{2}c_{j,1}^2 + \frac{1}{2}\varepsilon_{j,1}^2 + \frac{1}{2}c_{psj}^2 + \frac{1}{2}\varepsilon_{psj}^2 + \frac{d_j}{2\beta_j}\Theta_j^2.$

根据文献 [6,34,35], 利用动态面控制技术, 将虚拟控制器信号 $\alpha_{j,1}$ 进行滤波, 一阶滤波器的形式 如下:

$$\omega_{j,2}\dot{\alpha}_{j,2,f} + \alpha_{j,2,f} = \alpha_{j,1}, \quad \alpha_{j,2,f}(0) = \alpha_{j,1}(0), \tag{20}$$

其中, $\alpha_{j,2,f}$ 表示滤波器输出信号, $\omega_{j,2}$ 表示时间常数, 定义 $\chi_{j,2} = \alpha_{j,2,f} - \alpha_{j,1}$, 则 $\dot{\alpha}_{j,2,f} = -\frac{\chi_{j,2}}{\omega_{j,2}}$, 且 $\dot{\chi}_{j,2} = \dot{\alpha}_{j,2,f} - \dot{\alpha}_{j,1} = -\frac{\chi_{j,2}}{\omega_{j,2}} + D_{j,2}$,其中 $D_{j,2} = -\frac{\partial \alpha_{j,1}}{\partial x_{j,1}} (f_{j,1} + x_{j,2}) - \sum_{l=0}^{1} \frac{\partial \alpha_{j,1}}{\partial y_{dj}^{(l)}} y_{dj}^{(l+1)} - \frac{\partial \alpha_{j,1}}{\partial \hat{\theta}_{j}} \dot{\hat{\theta}}_{j} - \frac{\partial \alpha_{j,1}}{\partial \hat{\Theta}_{j}} \dot{\hat{\Theta}}_{j}$. 那么

$$\dot{V}_{j,1} \leqslant -k_{j,1}z_{j,1}^2 + \frac{1}{r_j}\tilde{\theta}_j \left[\frac{r_j}{2c_{j,1}^2} z_{j,1}^2 S^{\mathrm{T}}(Y_{j,1}) S(Y_{j,1}) - \dot{\hat{\theta}}_j \right] - \frac{d_j}{2\beta_j} \tilde{\Theta}_j^2 + \Xi_{j,1} + z_{j,1}\chi_{j,2} + z_{j,1}z_{j,2}$$

注释1 我们利用动态面控制技术将复杂的求偏导运算变成简单的代数运算,从而减少计算负担, 使控制器的设计过程变得简单,即在反步法控制设计的第 i pu (i = 1, 2, ..., m - 1)中引入一阶滤波器, 利用滤波器的输出信号 $\alpha_{j,i+1,f}$ 替代虚拟控制器 $\alpha_{j,i}$,在设计第 i+1步的虚拟控制器 $\alpha_{j,i+1}$ 时避免对 第 i步的虚拟控制器 $\alpha_{j,i}$ 求偏导.

步骤 $j, i \ (i = 2, 3, \dots, m - 1)$ 选取 Lyapunov 函数为

$$V_{j,i} = V_{j,i-1} + \frac{1}{2}z_{j,i}^2 + \frac{1}{2}\chi_{j,i}^2,$$

对 V_{j,i} 求导, 其导数为

$$\dot{V}_{j,i} \leqslant -\sum_{l=1}^{i-1} k_{j,l} z_{j,l}^2 + z_{j,i-1} z_{j,i} + z_{j,i} z_{j,i+1} + \sum_{l=1}^{i-1} z_{j,l} \chi_{j,l+1} + z_{j,i} (\alpha_{j,i+1,f} - \alpha_{j,i}) + \Xi_{j,i-1} + \sum_{l=2}^{i} \left(\frac{z_{j,l} \chi_{j,l}}{\omega_{j,l}} - \frac{\chi_{j,l}^2}{\omega_{j,l}} + \chi_{j,l} D_{j,l} \right) + \frac{1}{r_j} \tilde{\theta}_j \left[\sum_{l=1}^{i-1} \frac{r_j}{2c_{j,l}^2} z_{j,l}^2 S^{\mathrm{T}}(Y_{j,l}) S(Y_{j,l}) - \dot{\hat{\theta}}_j \right] - \frac{d_j}{2\beta_j} \tilde{\Theta}_j^2 + z_{j,i} (\bar{f}_{j,i}(\zeta_{j,i}) + \alpha_{j,i}),$$

$$(21)$$

其中, $\Xi_{j,i-1} = \frac{1}{2} \sum_{l=1}^{i-1} (c_{j,l}^2 + \varepsilon_{j,l}^2) + \frac{1}{2} c_{psj}^2 + \frac{1}{2} \varepsilon_{psj}^2 + \frac{d_j}{2\beta_j} \Theta_j^2$, $\zeta_{j,i} = x$, $\bar{f}_{j,i}(\zeta_{j,i}) = f_{j,i}$. 未知非线性 函数 $\bar{f}_{j,i}(\zeta_{j,i})$ 通过神经网络进行逼近, 类似地, $\bar{f}_{j,i}(\zeta_{j,i}) = W_{j,i}^{\mathrm{T}}S(\zeta_{j,i}) + \delta_{j,i}(\zeta_{j,i})$, 其中, $|\delta_{j,i}| \leq \varepsilon_{j,i}$, 且 $\varepsilon_{j,i} > 0$. 利用引理 1, 与式 (16) 类似, 可以得到

$$z_{j,i}\bar{f}_{j,i} \leqslant \frac{1}{2}z_{j,i}^2 + \frac{1}{2}c_{j,i}^2 + \frac{1}{2}\varepsilon_{j,i}^2 + \frac{1}{2}c_{j,i}^2 z_{j,i}^2\theta_j S^{\mathrm{T}}(Y_{j,i})S(Y_{j,i}),$$
(22)

其中, Y_{j,i} = x̄_{j,i} = [x_{j,1}, x_{j,2},..., x_{j,i}]^T. 将式 (22) 代入式 (21), 并根据式 (12), 可以得到

$$\begin{split} \dot{V}_{j,i} \leqslant &-\sum_{l=1}^{i} k_{j,l} z_{j,l}^{2} + z_{j,i} z_{j,i+1} + \sum_{l=1}^{i-1} z_{j,l} \chi_{j,l+1} + \frac{1}{r_{j}} \tilde{\theta}_{j} \left[\sum_{l=1}^{i} \frac{r_{j}}{2c_{j,l}^{2}} z_{j,l}^{2} S^{\mathrm{T}}(Y_{j,l}) S(Y_{j,l}) - \dot{\hat{\theta}}_{j} \right] \\ &+ \sum_{l=2}^{i} \left(\frac{z_{j,l} \chi_{j,l}}{\omega_{j,l}} - \frac{\chi_{j,l}^{2}}{\omega_{j,l}} + \chi_{j,l} D_{j,l} \right) + \Xi_{j,i} + z_{j,i} (\alpha_{j,i+1,f} - \alpha_{j,i}) - \frac{d_{j}}{2\beta_{j}} \tilde{\Theta}_{j}^{2}, \end{split}$$

其中, $\Xi_{j,i} = \frac{1}{2} \sum_{l=1}^{i} (c_{j,l}^2 + \varepsilon_{j,l}^2) + \frac{1}{2} c_{psj}^2 + \frac{1}{2} \varepsilon_{psj}^2 + \frac{d_j}{2\beta_j} \Theta_j^2.$ 类似地, 将虚拟控制器信号 $\alpha_{j,i}$ 进行滤波, 一阶滤波器的形式如下:

$$\omega_{j,i+1}\dot{\alpha}_{j,i+1,f} + \alpha_{j,i+1,f} = \alpha_{j,i}, \quad \alpha_{j,i+1,f}(0) = \alpha_{j,i}(0), \tag{23}$$

其中, $\alpha_{j,i+1,f}$ 表示滤波器输出信号, $\omega_{j,i+1}$ 表示时间常数. 设 $\chi_{j,i+1} = \alpha_{j,i+1,f} - \alpha_{j,i}$, 则 $\dot{\alpha}_{j,i+1,f} = -\frac{\chi_{j,i+1}}{\omega_{j,i+1}}$, 且 $\dot{\chi}_{j,i+1} = -\frac{\chi_{j,i+1}}{\omega_{j,i+1}} + D_{j,i+1}$, 其中 $D_{j,i+1} = -\sum_{l=0}^{1} \frac{\partial \alpha_{j,1}}{\partial y_{d_j}^{(l)}} y_{d_j}^{(l+1)} - \sum_{l=1}^{i} \frac{\partial \alpha_{j,i}}{\partial x_{j,l}} (f_{j,l} + x_{j,l+1}) - \frac{\partial \alpha_{j,i}}{\partial \hat{\theta}_j} \hat{\theta}_j$. 那么

$$\begin{split} \dot{V}_{j,i} \leqslant &-\sum_{l=1}^{i} k_{j,l} z_{j,l}^{2} + z_{j,i} z_{j,i+1} + \sum_{l=1}^{i} z_{j,l} \chi_{j,l+1} + \frac{1}{r_{j}} \tilde{\theta}_{j} \left[\sum_{l=1}^{i} \frac{r_{j}}{2c_{j,l}^{2}} z_{j,l}^{2} S^{\mathrm{T}}(Y_{j,l}) S(Y_{j,l}) - \dot{\theta}_{j} \right] \\ &+ \sum_{l=2}^{i} \left(\frac{z_{j,l} \chi_{j,l}}{\omega_{j,l}} - \frac{\chi_{j,l}^{2}}{\omega_{j,l}} + \chi_{j,l} D_{j,l} \right) + \Xi_{j,i} - \frac{d_{j}}{2\beta_{j}} \tilde{\Theta}_{j}^{2}. \end{split}$$

步骤 j,m 选取 Lyapunov 函数为

$$V_{j,m} = V_{j,m-1} + \frac{1}{2}z_{j,m}^2 + \frac{1}{2}\chi_{j,m}^2,$$

对 V_{j,m} 求导, 其导数为

$$\dot{V}_{j,m} \leqslant -\sum_{l=1}^{m-1} k_{j,l} z_{j,l}^{2} + z_{j,m-1} z_{j,m} + \sum_{l=1}^{m-1} z_{j,l} \chi_{j,l+1} + \frac{1}{r_{j}} \tilde{\theta}_{j} \left[\sum_{l=1}^{m-1} \frac{r_{j}}{2c_{j,l}^{2}} z_{j,l}^{2} S^{\mathrm{T}}(Y_{j,l}) S(Y_{j,l}) - \dot{\hat{\theta}}_{j} \right]$$
$$+ z_{j,m} (\bar{f}_{j,m}(\zeta_{j,m}) + u_{j}) - \frac{d_{j}}{2\beta_{j}} \tilde{\Theta}_{j}^{2} + \sum_{l=2}^{m} \left(\frac{z_{j,l} \chi_{j,l}}{\omega_{j,l}} - \frac{\chi_{j,l}^{2}}{\omega_{j,l}} + \chi_{j,l} D_{j,l} \right) + \Xi_{j,m-1}, \qquad (24)$$

其中, $\Xi_{j,m-1} = \frac{1}{2} \sum_{l=1}^{m-1} (c_{j,l}^2 + \varepsilon_{j,l}^2) + \frac{1}{2} c_{psj}^2 + \frac{1}{2} \varepsilon_{psj}^2 + \frac{d_j}{2\beta_j} \Theta_j^2$, $\zeta_{j,m} = x$, $\bar{f}_{j,m}(\zeta_{j,m}) = f_{j,m}$. 未知非 线性函数 $\bar{f}_{j,m}(\zeta_{j,m})$ 通过神经网络进行逼近, 类似地, $\bar{f}_{j,m}(\zeta_{j,m}) = W_{j,m}^T S(\zeta_{j,m}) + \delta_{j,m}(\zeta_{j,m})$, 其中, $|\delta_{j,m}| \leq \varepsilon_{j,m}$, 且 $\varepsilon_{j,m} > 0$. 利用引理 1, 与式 (16) 和 (22) 类似, 可以得到

$$z_{j,m}\bar{f}_{j,m} \leqslant \frac{1}{2}z_{j,m}^2 + \frac{1}{2}c_{j,m}^2 + \frac{1}{2}\varepsilon_{j,m}^2 + \frac{1}{2}c_{j,m}^2 z_{j,m}^2 \theta_j S^{\mathrm{T}}(Y_{j,m})S(Y_{j,m}),$$
(25)

其中, Y_{j,m} = x. 根据式 (6), (8), (9) 和假设 1, 可得

$$\underline{\alpha}_{j}\rho_{j}(t)\overline{\omega}_{j}(t) + \lambda_{j}(t) \leqslant (\bar{\alpha}_{j} - \underline{\alpha}_{j})M_{m} + \bar{\lambda}_{j}.$$
(26)

将式 (25) 和 (26) 代入式 (24), 可以得到

$$\dot{V}_{j,m} \leqslant -\sum_{l=1}^{m-1} k_{j,l} z_{j,l}^2 + z_{j,m-1} z_{j,m} + \sum_{l=1}^{m-1} z_{j,l} \chi_{j,l+1} + \frac{1}{2} z_{j,m}^2 + \sum_{l=2}^m \left(\frac{z_{j,l} \chi_{j,l}}{\omega_{j,l}} - \frac{\chi_{j,l}^2}{\omega_{j,l}} + \chi_{j,l} D_{j,l} \right)$$

$$+ \frac{1}{r_j} \tilde{\theta}_j \left[\sum_{l=1}^m \frac{r_j}{2c_{j,l}^2} z_{j,l}^2 S^{\mathrm{T}}(Y_{j,l}) S(Y_{j,l}) - \dot{\hat{\theta}}_j \right] + \frac{1}{2c_{j,m}^2} z_{j,m}^2 \hat{\theta}_j S^{\mathrm{T}}(Y_{j,m}) S(Y_{j,m}) - \frac{d_j}{2\beta_j} \tilde{\Theta}_j^2$$

+ $\Xi_{j,m} + z_{j,m} \left[\underline{\alpha}_j \overline{\omega}_j(t) + (\bar{\alpha}_j - \underline{\alpha}_j) M_m + \bar{\lambda}_j \right],$

其中, $\Xi_{j,m} = \frac{1}{2} \sum_{l=1}^{m} (c_{j,l}^2 + \varepsilon_{j,l}^2) + \frac{1}{2} c_{psj}^2 + \frac{1}{2} \varepsilon_{psj}^2 + \frac{d_j}{2\beta_j} \Theta_j^2$. 对 $z_{j,m} \bar{\lambda}_j$ 使用 Young's 不等式放缩, 可得

$$z_{j,m}\bar{\lambda}_j \leqslant \frac{z_{j,m}^2}{2} + \frac{\bar{\lambda}_j^2}{2}.$$
(27)

根据式 (13), (14) 和 (27), 可得

$$\dot{V}_{j,m} \leqslant -\sum_{l=1}^{m} k_{j,l} z_{j,l}^{2} + \sum_{l=1}^{m-1} z_{j,l} \chi_{j,l+1} - \frac{d_{j}}{2\beta_{j}} \tilde{\Theta}_{j}^{2} + \sum_{l=2}^{m} \left(\frac{z_{j,l} \chi_{j,l}}{\omega_{j,l}} - \frac{\chi_{j,l}^{2}}{\omega_{j,l}} + \chi_{j,l} D_{j,l} \right) + \Xi_{j,m} + \frac{b_{j}}{r_{j}} \tilde{\theta}_{j} \hat{\theta}_{j} + \frac{z_{j,m}^{2}}{2} + \frac{\bar{\lambda}_{j}^{2}}{2}.$$
(28)

使用 Young's 不等式, 可得

$$\sum_{l=1}^{m-1} z_{j,l} \chi_{j,l+1} \leqslant \sum_{l=1}^{m-1} \frac{1}{2} z_{j,l}^2 + \sum_{l=2}^m \frac{1}{2} \chi_{j,l}^2, \tag{29}$$

$$\frac{b_j}{r_j}\tilde{\theta}_j\hat{\theta}_j \leqslant -\frac{b_j}{2r_j}\tilde{\theta}_j^2 + \frac{b_j}{2r_j}\theta_j^2,\tag{30}$$

$$\sum_{l=2}^{m} \left(\frac{z_{j,l}\chi_{j,l}}{\omega_{j,l}} - \frac{\chi_{j,l}^2}{\omega_{j,l}} + \chi_{j,l}D_{j,l} \right) \leqslant \sum_{l=2}^{m} \left(\frac{z_{j,l}^2}{2\omega_{j,l}} - \frac{\chi_{j,l}^2}{2\omega_{j,l}} + \frac{\chi_{j,l}^2D_{j,l}^2}{2\pi_j} + \frac{\pi_j}{2} \right), \tag{31}$$

其中, π_j > 0 为设计参数. 将式 (29)~(31) 代入式 (28), 可得

$$\dot{V}_{j,m} \leqslant -\left(k_{j,1} - \frac{1}{2}\right) z_{j,1}^2 - \sum_{l=2}^m \left(k_{j,l} - \frac{1}{2} - \frac{1}{2\omega_{j,l}}\right) z_{j,l}^2 + \bar{\Xi}_{j,m} - \sum_{l=2}^m \left(-\frac{1}{2} + \frac{1}{2\omega_{j,l}} - \frac{D_{j,l}^2}{2\pi_j}\right) \chi_{j,l}^2 - \frac{b_j}{2r_j} \tilde{\theta}_j^2 - \frac{d_j}{2\beta_j} \tilde{\Theta}_j^2,$$

其中, $\overline{\Xi}_{j,m} = \Xi_{j,m} + \frac{\pi_j(m-1)}{2} + \frac{b_j}{2r_j}\theta_j^2 + \frac{\overline{\lambda}_j^2}{2}.$ 选取系统的 Lyapunov 函数为

$$V = \sum_{j=1}^{n} V_{j,m}.$$

对 V 进行求导, 可得

$$\dot{V} \leqslant \sum_{j=1}^{n} \left[-\left(k_{j,1} - \frac{1}{2}\right) z_{j,1}^{2} - \sum_{l=2}^{m} \left(k_{j,l} - \frac{1}{2} - \frac{1}{2\omega_{j,l}}\right) z_{j,l}^{2} - \sum_{l=2}^{m} \left(-\frac{1}{2} + \frac{1}{2\omega_{j,l}} - \frac{D_{j,l}^{2}}{2\pi_{j}}\right) \chi_{j,l}^{2} - \frac{b_{j}}{2r_{j}} \tilde{\theta}_{j}^{2} - \frac{d_{j}}{2\beta_{j}} \tilde{\Theta}_{j}^{2} \right] + \Delta,$$

$$(32)$$

其中, $\Delta = \sum_{j=1}^{n} \overline{\Xi}_{j,m}$.

那么,式 (32) 可以写成

$$\dot{V} \leqslant -CV + \Delta.$$
 (33)

对不等式 (33) 两边同时积分可得

$$0 \leqslant V(t) \leqslant V(0) \mathrm{e}^{-Ct} + \frac{\Delta}{C},\tag{34}$$

由式 (34) 可得闭环系统中的所有信号都是半全局一致最终有界的. 从而可得

$$\lim_{t \to \infty} |z_{j,1}| \leq \lim_{t \to \infty} \sqrt{2V(0)e^{-Ct} + \frac{2\Delta}{C}} \leq \sqrt{\frac{2\Delta}{C}},\tag{35}$$

因此, 由式 (35) 可知, 通过选择适当的设计参数, 使 C 足够大或者 Δ 足够小, 则能使系统的跟踪误差 收敛至原点附近的紧集内.

定理1 针对一类具有传感器故障和输入死区的非严格反馈非线性系统 (1), 设计虚拟控制器 (10), (12), 实际控制器 (13), 一阶滤波器 (20), (23) 及自适应律 (11), (14), 通过选择合适的参数使得闭环系 统内所有信号都是半全局一致最终有界的, 且能使跟踪误差收敛至原点附近的紧集内.

根据以上的分析,提出自适应神经网络容错控制的设计算法^[36],如算法1所示.

Algorithm 1

Step 1. Determine the number of neural network nodes ι , and design the Gaussian function $S_i(\zeta)$.

Step 2. Based on Step 1, define the neural network $W^{T}S(\zeta)$ to identify the nonlinear functions of the MIMO systems (1).

Step 3. Select appropriate design parameters $k_{j,1} > 0$, $c_{j,1} > 0$, $c_{psj} > 0$, $\beta_j > 0$, $d_j > 0$, and design virtual control signal $\alpha_{j,1}$ (10), adaptive law $\dot{\hat{\Theta}}_j$ (11) and first-order filter (20), where j = 1, 2, ..., n.

Step 4. Provide approximate design parameters $k_{j,i} > 0$, $c_{j,i} > 0$, and design virtual control signals $\alpha_{j,i}$ (12) and first-order filter (23), where i = 2, 3, ..., m - 1.

Step 5. Choose appropriate design parameters $k_{j,m} > 0, c_{j,m} > 0, r_j > 0, b_j > 0$, and determine the actual control signal $\overline{\omega}_j(t)$ (13) and adaptive law $\dot{\hat{\theta}}_j$ (14) for the MIMO nonlinear systems (1).

4 仿真算例

仿真 1. 通过一个数值仿真实验的结果验证本文所提出的控制方法的有效性,考虑如下三阶系统:

$$\dot{x}_{j,i} = f_{j,i} + x_{j,i+1},$$

 $\dot{x}_{j,m} = f_{j,m} + u_j,$
 $y_j = K_j x_{j,1} + q_j,$

其中, j = 1, 2, i = 1, 2, m = 3, 非线性函数 $f_{1,1} = \frac{x_{1,1}x_{1,2}}{2} + \frac{1}{10(1+x_{1,3}^2)} + \frac{1}{2+x_{2,1}^2}$, $f_{1,2} = x_{1,1}x_{1,2}x_{1,3} + \frac{1}{1+x_{2,3}^2}$, $f_{1,3} = -x_{1,2}(\sin(x_{1,3}))^2 + x_{2,3} + \frac{1}{1+x_{1,1}^2}$, $f_{2,1} = \frac{x_{2,1}x_{2,2}}{2} + \frac{1}{10(1+x_{2,3}^2)} + \frac{1}{2+x_{1,2}^2}$, $f_{2,2} = x_{2,1}x_{2,2}x_{2,3} + \frac{1}{1+x_{1,3}^2}$, $f_{2,3} = -x_{2,2}(\sin(x_{2,3}))^2 + x_{1,3} + \frac{1}{1+x_{2,1}^2}$. 假设系统的参考信号为: $y_{d1} = y_{d2} = \sin(t)$.

根据上述系统, 选取适当的设计参数为: $c_{1,1} = c_{2,1} = 15$, $c_{1,2} = c_{2,2} = 18$, $c_{1,3} = c_{2,3} = 0.5$, $k_{1,1} = 24$, $k_{1,2} = 85$, $k_{1,3} = 100$, $k_{2,1} = 18$, $k_{2,2} = 75$, $k_{2,3} = 100$, $c_{ps1} = c_{ps2} = 1.5$, $r_1 = r_2 = 0.1$, $\beta_1 = 9$, $\beta_2 = 12$, $b_1 = b_2 = 3.2$, $d_1 = d_2 = 2$, $\omega_{1,2} = 0.08$, $\omega_{1,3} = 0.01$, $\omega_{2,2} = 0.32$, $\omega_{2,3} = 0.012$,



图 3 (网络版彩图) 仿真 1 输出信号 y_j 和参考信号 y_{dj} Figure 3 (Color online) (a) Output y_1 and reference signal y_{d1} ; (b) output y_2 and reference signal y_{d2} in simulation 1.



图 5 (网络版彩图) 仿真 1 死区输入 ϖ_1 与死区输出 u_1 Figure 5 (Color online) Dead zone input ϖ_1 and dead zone output u_1 in simulation 1.



图 4 (网络版彩图) 仿真 1 自适应参数 (a) $\hat{\theta}_1$ 和 (b) $\hat{\theta}_2$ Figure 4 (Color online) Adaptive parameters (a) $\hat{\theta}_1$ and (b) $\hat{\theta}_2$ in simulation 1.



图 6 (网络版彩图) 仿真 1 死区输入 ϖ_2 与死区输出 u_2 Figure 6 (Color online) Dead zone input ϖ_2 and dead zone output u_2 in simulation 1.

 $M_{m1} = M_{m2} = 580.$ 选取适当的传感器故障参数为: $K_1 = K_2 = 0.9, q_1 = q_2 = 0.$ 选取不对称输入死 区的参数为: $o_{1r} = o_{2r} = 2.65, o_{1l} = o_{2l} = 2.15, p_{1r} = p_{2r} = p_{1l} = p_{2l} = 5.4.$ 系统的初始状态取值如下: $[x_{1,1}(0), x_{1,2}(0), x_{1,3}(0), x_{2,1}(0), x_{2,2}(0), x_{2,3}(0)]^{\mathrm{T}} = [0.01, 0.01, 0.01, 0.01, 0.01]^{\mathrm{T}}.$ 假设自适应参数的 初始状态为: $\hat{\theta}_1(0) = \hat{\theta}_2(0) = 0, \hat{\Theta}_{ps1}(0) = \hat{\Theta}_{ps2}(0) = 0.$

仿真结果如图 3~6 所示. 图 3(a) 表示输出信号 y_1 与参考信号 y_{d1} 的跟踪效果图, 图 3(b) 表示输 出信号 y_2 与参考信号 y_{d2} 的跟踪效果图, 由图 3 可知, 从 t = 20 s 开始, 系统发生传感器故障, 有容 错的控制方案使系统的输出信号 (红色实线) 仍能较好地跟踪上参考信号 (黑色虚线), 而无容错的控 制方案无法使系统的输出信号 (蓝色点划线) 跟踪上参考信号 (黑色虚线). 图 4(a) 和 (b) 分别表示自 适应参数 $\hat{\theta}_1$ 和 $\hat{\theta}_2$ 的响应曲线, 图 5 表示系统的死区输入信号 ϖ_1 和死区输出信号 u_1 的轨迹图, 图 6 表示系统的死区输入信号 ϖ_2 和死区输出信号 u_2 的轨迹图. 由图 4~6 可知, 当 t = 20 s 时, 自适应参



图 7 (网络版彩图) 仿真 2 输出信号 y_j 和参考信号 y_{dj} **Figure 7** (Color online) (a) Output y_1 and reference signal y_{d1} ; (b) output y_2 and reference signal y_{d2} in simulation 2.



图 9 (网络版彩图) 仿真 2 死区输入 ϖ_1 与死区输出 u_1 Figure 9 (Color online) Dead zone input ϖ_1 and dead zone output u_1 in simulation 2.



图 8 (网络版彩图) 仿真 2 自适应参数 (a) $\hat{\theta}_1$ 和 (b) $\hat{\theta}_2$ Figure 8 (Color online) Adaptive parameters (a) $\hat{\theta}_1$ and (b) $\hat{\theta}_2$ in simulation 2.



图 10 (网络版彩图) 仿真 2 死区输入 ϖ_2 与死区输 出 u_2

Figure 10 (Color online) Dead zone input ϖ_2 and dead zone output u_2 in simulation 2.

数 $\hat{\theta}_1$, $\hat{\theta}_2$, 死区输入信号 ϖ_1 , ϖ_2 和死区输出信号 u_1 , u_2 出现短暂的跳变, 但在 t = 20 s 后仍能保持 有界.

仿真 2. 根据文献 [31], 具有传感器故障和输入死区的双倒立摆系统的动力学方程如下所示:

$$\begin{aligned} \dot{x}_{j,1} &= x_{j,2} + f_{j,1}(x), \\ \dot{x}_{j,2} &= \frac{u_j}{J_j} + A_j + f_{j,2}(x), \\ y_j &= K_j x_{j,1} + q_j, \end{aligned}$$

其中, $j = 1, 2, A_1 = -\frac{nh^2}{4J_1}\sin(x_{2,1}), A_2 = -\frac{nh^2}{2J_2}\sin(x_{1,2}),$ 系统的参考信号为: $y_{d1} = 4\sin(\frac{t}{2}) + 2\sin(t),$

 $y_{d2} = 5\cos(\frac{t}{2}) + \cos(2t)$. 假设 $f_{1,1}(x) = f_{2,1}(x) = 0$, $f_{1,2}(x) = \frac{2nh^2}{4J_1}\sin(x_{2,1}) + (\frac{m_1gh}{J_1} - \frac{nh^2}{4J_1})\sin(x_{1,1}) + \frac{nh(L-e)}{2J_1}$, $f_{2,2}(x) = \frac{3nh^2}{4J_2}\sin(x_{1,2}) + (\frac{m_2gh}{J_2} - \frac{nh^2}{4J_2})\sin(x_{2,1}) + \frac{nh(L-e)}{2J_2}$, $m_1 = m_2 = 2$ kg 表示连杆的末端质 量, n = 10 N/m 表示弹簧的劲度系数, $J_1 = J_2 = 6$ kg·m² 表示连杆的转动惯量, h = 0.1 m 表示连杆 的高度, g = 9.81 m/s² 表示重力加速度, L = 0.5 m 表示弹簧的原长, 两个连杆之间的距离为 e = 0.4 m, 且 e < L.

选取适当的设计参数为: $c_{1,1} = c_{1,2} = 10$, $c_{2,1} = c_{2,2} = 50$, $c_{ps1} = c_{ps2} = 25$, $r_1 = 0.1$, $r_2 = 0.01$, $\beta_1 = \beta_2 = 8$, $b_1 = b_2 = 0.1$, $d_1 = d_2 = 1$, $k_{1,1} = k_{1,2} = k_{2,1} = k_{2,2} = 15$, $\omega_{1,2} = 0.01$, $\omega_{2,2} = 0.02$, $M_{m1} = M_{m2} = 1000$. 选取适当的传感器故障参数为: $K_1 = K_2 = 0.9$, $q_1 = q_2 = 0$. 选取适当的 死区参数为: $p_{1r} = p_{1l} = 10$, $p_{2r} = p_{2l} = 10$, $o_{1r} = o_{2r} = 2$, $o_{1l} = o_{2l} = 2.1$. 假设自适应参数的 初始状态如下: $\hat{\theta}_1(0) = \hat{\theta}_2(0) = 0$, $\hat{\Theta}_{ps1}(0) = \hat{\Theta}_{ps2}(0) = 0$, 上述非线性系统的初始状态取值如下: $[x_{1,1}(0), x_{1,2}(0), x_{2,1}(0), x_{2,2}(0)]^{\mathrm{T}} = [0.01, 0.01, 0.01, 0.01]^{\mathrm{T}}$. 由图 7~10 可知, 双倒立摆系统在受传感器 故障和输入死区影响的情况下,本文所提出的自适应神经网络容错控制方法仍能保证系统的稳定性, 并能获得较好的跟踪效果.

5 结论

本文针对一类具有非严格反馈形式的多输入多输出非线性系统,在同时发生传感器故障和不对称 输入死区的情况下,结合反步法和动态面控制技术设计了一种自适应神经网络容错控制方案.在不需 构造死区逆模型的基础上,利用死区斜率的有界性有效地减小了输入死区对非线性系统造成的影响. 基于 Lyapunov 稳定性理论,保证了闭环系统中的所有信号都是有界的,并通过两个仿真例子验证了 该方法的有效性.

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Adaptive neural network fault-tolerant control for MIMO systems with dead zone inputs

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Abstract In this paper, an adaptive neural network fault-tolerant control (FTC) strategy is proposed for a class of multi-input and multi-output (MIMO) nonlinear systems in nonstrict-feedback form, in which sensor faults and nonsymmetric dead zone inputs are considered. Based on the backstepping method, the desired controller is designed. The adaptive neural network control approach is proposed to handle the problem of sensor faults. The effect of dead zone inputs on the system performance can be compensated by virtue of the boundedness of dead zone slopes. Furthermore, the dynamic surface control technique is introduced to prevent an "explosion of complexity". The proposed control method ensures that all the signals of the closed-loop system are semi-globally uniformly ultimately bounded, and that the tracking errors converge to a compact set around the origin. Finally, simulation results are provided to demonstrate the effectiveness of the proposed approach.

Keywords nonlinear systems, sensor faults, fault-tolerant control, dynamic surface control, dead zone inputs



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